LS-DYNA® KEYWORD USER'S MANUAL

VOLUME III

Multi-Physics Solvers

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LS-DYNA MULTIPHYSICS USER'S MANUAL INTRODUCTION

In this manual, there are five main solvers: two compressible flow solvers, an incompressible flow solver, an electromagnetism solver, and a battery electrochemistry solver. Each of them implements coupling with the structural solver in LS-DYNA.

The keywords covered in this manual fit into one of three categories. In the first category are the keyword cards that provide input to each of the multiphysics solvers that in turn couple with the structural solver. In the second category are keyword cards involving extensions to the basic solvers. Presently, the chemistry and stochastic particle solvers are the two solvers in this category, and they are used in conjunction with the *CESE compressible flow solver discussed below. In the third category are keyword cards for support facilities. A volume mesher that creates volume tetrahedral element meshes from bounding surface meshes is one of these tools. Another is a data output mechanism for a limited set of variables from some of the solvers in this manual. This mechanism is accessed through *LSO keyword cards.

The CESE solver is a compressible flow solver based upon the Conservation Element/Solution Element (CE/SE) method, originally proposed by Chang of the NASA Glenn Research Center. This method is a novel numerical framework for conservation laws. It has many non-traditional features, including a unified treatment of space and time, the introduction of separate conservation elements (CE) and solution elements (SE), and a novel shock capturing strategy without using a Riemann solver. This method has been used to solve many types of flow problems, such as detonation waves, shock/acoustic wave interaction, cavitating flows, supersonic liquid jets, and chemically reacting flows. In LS-DYNA, it has been extended to also solve fluidstructure interaction (FSI) problems. It does this with two approaches. The first approach solves the compressible flow equations on an Eulerian mesh while the structural mechanics is solved on a moving mesh that moves through the fixed CE/SE mesh. In the second approach (new with this version), the CE/SE mesh moves in a fashion such that its FSI boundary surface matches the corresponding FSI boundary surface of the moving structural mechanics mesh. This second approach is more accurate for FSI problems, especially with boundary layers flows. Another feature with the CESE moving mesh solver is conjugate heat transfer coupling with the solid thermal solver. The chemistry and stochastic particle solvers are two addon solvers that extend the CESE solver.

The dual CESE solver is another compressible flow solver that is also based upon the Conservation Element/Solution Element (CE/SE) method, but with improvements related to accuracy and robustness. This method follows a similar novel numerical framework for conservation laws. In LS-DYNA, the dual CESE solver also include fluid-structure interaction (FSI) capabilities. It also does this with two approaches. The first approach solves the compressible flow equations on an Eulerian mesh while the structural mechanics is solved on a moving mesh that moves through the fixed dual CE/SE mesh. In the second approach. the dual CE/SE mesh moves in a fashion such that its FSI boundary surface matches the corresponding FSI boundary surface of the moving structural mechanics mesh. This second approach is more accurate for FSI problems, especially with boundary layers flows. One of the advances in these FSI computations with the dual CESE solver as compared with the older CESE solver is that each FSI approach (or fixed mesh Eulerian solver) may be employed in different subregions of the fluid mesh in the same problem. Unlike the *CESE solvers, the dual CESE solvers do not yet have conjugate heat transfer coupling with the solid thermal solver, nor coupling with the chemistry or stochastic particle solvers. Another advance available only with the dual CESE solvers is the availability of equations of state for pure and pseudo-pure fluids of industrial interest in the REFPROP and COOLPROP EOS libraries. These complex EOSes are generally expensive to evaluate, so a bi-cubic table look-up mechanism has been developed that greatly accelerates their use.

The third solver is the incompressible flow solver (ICFD) that is fully coupled with the solid mechanics solver. This coupling permits robust FSI analysis via either an explicit technique when the FSI is weak, or using an implicit coupling when the FSI coupling is strong. In addition to being able to handle free surface flows, there is also a bi-phasic flow capability that involves modeling using a conservative Lagrangian interface tracking technique. Basic turbulence models are also supported. This solver is the first in LS-DYNA to make use of a new volume mesher that takes surface meshes bounding the fluid domain as input (*MESH keywords). In addition, during the time advancement of the incompressible flow, the solution is adaptively re-meshed as an automatic feature of the solver. Another important feature of the mesher is the ability to create boundary layer meshes. These anisotropic meshes become a crucial part of the model when shear stresses are to be calculated near fluid walls. The ICFD solver is also coupled to the solid thermal solver using a monolithic approach for conjugate heat transfer problems.

The fourth solver is an electromagnetics (EM) solver. This module solves the Maxwell equations in the Eddy current (induction-diffusion) approximation. This is suitable for cases where the propagation of electromagnetic waves in air (or vacuum) can be considered as instantaneous. Therefore, the wave propagation is not solved. The main applications are Magnetic Metal Forming, bending or welding, induced heating, ring expansions and so forth. The EM module allows the introduction of a source of electrical current into solid conductors and the computation of the associated magnetic field, electric field, as well as induced currents. The EM solver is coupled with the structural mechanics solver (the Lorentz forces are added to the mechanics equations of motion), and with the structural thermal solver (the ohmic heating is added to the thermal solver as an extra source of heat). The EM fields are solved using a Finite

Element Method (FEM) for the conductors and a Boundary Element Method (BEM) for the surrounding air/insulators. Thus no air mesh is necessary.

The fifth solver is a battery electrochemistry solver. At this time, the available capability involves a one-dimensional electrochemistry solver that is coupled to the structural mechanics and structural thermal solver in each structural element identified as being part of a battery cell. It solves these one-dimensional models implicitly so as to be able to run simulations for very long physical times that are typical of batterystructure interaction problems.

As stated above, the *CHEMISTRY and *STOCHASTIC cards are only used in the CESE solver at this time.

*BATTERY

The keyword *BATTERY provides input data for the electrochemistry solver:

*BATTERY_ECHEM_CELL_GEOMETRY *BATTERY_ECHEM_CONTROL_SOLVER *BATTERY_ECHEM_INITIAL *BATTERY_ECHEM_MAT_ANODE *BATTERY_ECHEM_MAT_CATHODE *BATTERY_ECHEM_MAT_ELECTROLYTE *BATTERY_ECHEM_PART *BATTERY_ECHEM_THERMAL

For now, the available capability involves a one-dimensional electrochemistry solver that is coupled to the structural mechanics and structural thermal solver in each structural element identified as being part of a battery cell.

*BATTERY_ECHEM_CELL_GEOMETRY

Purpose: Set general-purpose geometry variables for a single cell BATTERY model.

Remarks:

1. The battery model identifier (IMODEL) should match the IMODEL value specified in the corresponding *BATTERY_ECHEM_CONTROL_SOLVER card. In case a different value is given, the value on the *BATTERY_ECHEM_- CONTROL_SOLVER card will be the default.

*BATTERY_ECHEM_CONTROL_SOLVER

Purpose: Set general purpose control variables for a BATTERY simulation.

VARIABLE DESCRIPTION

IMODEL Sets the battery model. EQ.1: A single insertion model EQ.2: Dual insertion model EQ.3: Non-porous model (not working) IGEOM Sets the geometric dimension: EQ.1: A single cell (1D) problem EQ.2: Two-dimensional (2D) problem (not working) EQ.3: Three-dimensional (3D) problem (not working) EQ.101: A single cell with thermal coupling

Remarks:

- 1. Default simulation for the Battery model is galvanostatic charge/discharge mode. A potentiostatic mode is simulated by running the galvanostatic mode until the desired cell potential is achieved via iteration of the cell current density. Currently, this is not working.
- 2. When the number of cycles is more than 1, one "Card 2" must be included for each of the cycles.
- 3. When LCUR is equal to 1, the value of CURV will be the initial current to run.

*BATTERY_ECHEM_INITIAL

Purpose: Initializes all simulation mesh points in the composite electrodes and electrolyte in every element of the BATTERY.

*BATTERY_ECHEM_MAT_ANODE

Purpose: Set the battery material variables for the anode side electrode.

PROPERTY Card.

POROCITY Card.

VARIABLE DESCRIPTION

PID Part number identifier

*BATTERY_ECHEM_MAT_ANODE *BATTERY

*BATTERY_ECHEM_MAT_CATHODE

Purpose: Set the battery material variables for the positive electrode.

PROPERTY Card.

POROCITY Card.

VARIABLE DESCRIPTION

PID Part number identifier

*BATTERY_ECHEM_MAT_CATHODE *BATTERY

*BATTERY_ECHEM_MAT_ELECTROLYTE

Purpose: Set the battery material variables for the electrolyte and separator.

POROCITY Card In Separator.

Battery Cell Output File (an ASCII file) Card.

VARIABLE DESCRIPTION

PID Part number identifier IELYTE Material identifier for the open-circuit potential. EQ.1: Lithium Hexafluoroarsenate in Methyl acetate, LiAsF6. EQ.2: Perchlorate in poly ethylene oxide (PEO). EQ.3: Sodium Triflate, CF3NaO3S in PEO. EQ.4: Lithium Hexafluoroarsenate in propylene carbonate

*BATTERY_ECHEM_PART

Purpose: Set the material and EOS identifiers for the BATTERY solver.

*BATTERY_ECHEM_THERMAL

Purpose: Set parameters for the thermal treatment in a cell stack.

Remarks:

- 1. In case of thermal-mechanical coupling, the part number for the battery simulation must be specified, so only this part number is considered in the battery parts.
- 2. If TID is 2, these values are set through the THERMAL Material card. including anisotropic conductivities (see *MAT_THERMAL_ORTHOTROPIC).

Example:

The following is a partial example for 1D Electrochemisty.

```
*Keyword 
\mathsf{S}*TITLE 
1D battery models 
$ 
*BATTERY_ECHEM_CONTROL_SOLVER 
$--------1---------2---------3---------4---------5---------6---------7 
$ model_id idimen runmod icycle 
 2 1 1 1 
$ o_mode itype o_curt r_time cutv 
 1 1 1 1 2.0 
$ 
*BATTERY_ECHEM_CELL_GEOMETRY 
$--------1---------2---------3---------4---------5---------6---------7 
$ model_id anode_l separ_l cathode_l acoll_l ccoll_l 
 1 1.0e-4 2.5e-5 1.0e-4 2.5e-5 2.5e-5 
$ na_mesh ns_mesh np_mesh 
   80 40 80 
\ddot{\varsigma}*BATTERY_ECHEM_INITIAL 
$--------1---------2---------3---------4---------5---------6---------7 
$ echemid mid 
   echeml batt_matl 
$ Li_con solid_c PHI2 PHIl curric pw_flux hic 
 1000.0 0.0 0.05 0.0 5.0 -1.0e-7 
\mathcal{S}*BATTERY_ECHEM_MAT_ANODE 
$--------1---------2---------3---------4---------5---------6---------7 
$ a_pid aocp_id capatl s_xa s_radl rate_c ranode 
 2 4 372.2 0.6 10.0e-6 1.0e-5 0.0 
$ rhoea rhofa rhocca diff_a con_a 
 1800.0 1800.0 8954.0 3.9e-14 100.0 
$ vfela vfpla vffia vfgsa 
 0.3 0.0 0.1 0.0 
\ddot{\mathsf{s}}*BATTERY_ECHEM_MAT_CATHODE<br>$--------1---------2---------3---------4---------5--------6---------7
$--------1---------2---------3---------4---------5---------6---------7 
$ c_pid cocp_id capat3 s_yc s_rad3 rate_c rcathoe 
 2 3 274.0 0.5 10.0e-6 3.0e-11 0.0 
$ rhoec rhofc rhoccc diff_c con_c 
 5010.0 1800.0 2707.0 1.0e-13 10.0 
$ vfelc vfplc vffic vfgsx 
 0.3 0.0 0.2 0.0 
\ddot{\mathcal{S}}*BATTERY_ECHEM_MAT_ELECTROLYTE 
$--------1---------2---------3---------4---------5---------6---------7 
$ elyt_pid elyte_id etype rhoel rhopl rhose cl_max 
 2 8 0 1324.0 1780.0 2000.0 8500.0
```
*BATTERY_ECHEM_THERMAL

*CESE

The keyword *CESE provides input data for the Conservation Element/Solution Element (CESE) compressible fluid solver:

*CESE_BOUNDARY_AXISYMMETRIC_{OPTION}

*CESE_BOUNDARY_BLAST_LOAD}

*CESE_BOUNDARY_CONJ_HEAT_{OPTION}

*CESE_BOUNDARY_CYCLIC_{OPTION}

*CESE_BOUNDARY_FSI_{OPTION}

*CESE_BOUNDARY_NON_REFLECTIVE_{OPTION}

*CESE_BOUNDARY_PRESCRIBED_{OPTION}

*CESE_BOUNDARY_REFLECTIVE_{OPTION}

*CESE_BOUNDARY_SLIDING_{OPTION}

*CESE_BOUNDARY_SOLID_WALL_{OPTION1}_{OPTION2}

*CESE_CHEMISTRY_D3PLOT

*CESE_CONTROL_LIMITER

*CESE_CONTROL_MESH_MOV

*CESE_CONTROL_SOLVER

*CESE_CONTROL_TIMESTEP

*CESE_DATABASE_ELOUT

*CESE_DATABASE_FLUXAVG

*CESE_DATABASE_FSIDRAG

*CESE_DATABASE_POINTOUT

*CESE_DATABASE_SSETDRAG

*CESE_DEFINE_NONINERTIAL

*CESE_DEFINE_POINT

*CESE_DRAG

*CESE_EOS_CAV_HOMOG_EQUILIB_

*CESE_EOS_IDEAL_GAS

*CESE_EOS_INFLATOR1

*CESE_EOS_INFLATOR2

*CESE_FSI_EXCLUDE

*CESE_INITIAL

*CESE_INITIAL_{OPTION}

*CESE_INITIAL_CHEMISTRY

*CESE_INITIAL_CHEMISTRY_ELEMENT

*CESE_INITIAL_CHEMISTRY_PART

*CESE_INITIAL_CHEMISTRY_SET

*CESE_MAT_000

*CESE_MAT_001 (*CESE_MAT_GAS)

*CESE_MAT_002

*CESE_PART

*CESE_SURFACE_MECHSSID_D3PLOT

*CESE_SURFACE_MECHVARS_D3PLOT

Note that when performing a chemistry calculation with the CESE solver, initialization should only be done with the *CESE_INITIAL_CHEMISTRY_… cards, not the *CESE_- INITIAL… cards.

*CESE_BOUNDARY_AXISYMMETRIC_OPTION

Available options are

MSURF

MSURF_SET

SFT

SEGMENT

Purpose: Define an axisymmetric boundary condition on the axisymmetric axis for the 2D axisymmetric CESE compressible flow solver.

The MSURF and MSURF_SET options are used when the CESE mesh has been created using *MESH cards. The SET and SEGMENT cards are used when *ELEMENT_SOLID cards are used to define the CESE mesh.

Surface Part Card. Card 1 format used when the MSURF keyword option is active. Provide as many cards as necessary. This input ends at the next keyword ("*") card.

Surface Part Set Card. Card 1 format used when the MSURF_SET keyword option is active. Provide as many cards as necessary. This input ends at the next keyword ("*") card.

Set Card. Card 1 format used when the SET keyword option is active. Provide as many cards as necessary. This input ends at the next keyword ("*") card.

Segment Cards. Card 1 format used when SEGMENT keyword option is active. Include an additional card for each corresponding pair of segments. This input ends at the next keyword ("*") card.

VARIABLE DESCRIPTION

Remarks:

1. This boundary condition can only be used on the axisymmetric axis for the 2D axisymmetric CESE fluid solver.

*CESE_BOUNDARY_**BLAST_LOAD**_OPTION

Available options include:

MSURF

MSURF_SET

SET

SEGMENT

Purpose: For the CESE compressible flow solver, set boundary values for velocity, density, and pressure from a blast wave defined by a *LOAD_BLAST_ENHANCED card. Boundary values are applied at the centroid of elements connected with this boundary. OPTION = SET and OPTION = SEGMENT are for user defined meshes whereas OPTION = MSURF or MSURF_SET are associated with the automatic volume mesher (See *MESH keywords).

That is, the MSURF and MSURF_SET options are used when the CESE mesh has been created using *MESH cards. The SET and SEGMENT cards are used when *ELE-MENT_SOLID cards are used to define the CESE mesh.

Card 1a		$\overline{2}$	3	$\overline{4}$	5	6	8
Variable	BID	MSURFID					
Type							
Default	none	none					

Surface Part Card. Card 1 format used when the MSURF keyword option is active.

Surface Part Set Card. Card 1 format used when the MSURF_SET keyword option is active.

Segment Card. Card 1 for SEGMENT keyword option is active.

*CESE_BOUNDARY_CONJ_HEAT_OPTION

Available options are:

MSURF MSURF_SET SET

SEGMENT

Purpose: Define a conjugate heat transfer interface condition for CESE compressible flows. This condition identifies those boundary faces of the CESE mesh that are in contact with non-moving structural parts, and through which heat flows. This is only possible when the structural thermal solver is also in being used in the structural parts.

The MSURF and MSURF_SET options are used when the CESE mesh has been created using *MESH cards. The SET and SEGMENT cards are used when *ELEMENT_SOLID cards are used to define the CESE mesh.

Surface Part Card. Card 1 used when the MSURF keyword option is active. Include as many cards as necessary. This input ends at the next keyword ("*") card.

Surface Part Set Card. Card 1 used when the MSURF_SET keyword option is active. Include as many cards as necessary. This input ends at the next keyword ("*") card.

Set Card. Card 1 used when the SET keyword option is active. Include as many cards as necessary. This input ends at the next keyword ("*") card.

Card 1c		$\overline{2}$	3	4	5	6	8
Variable	SSID						
Type							
Default	none						

Segment Cards. Card 1 used when SEGMENT keyword option is active. Include an additional card for each corresponding pair of segments. This input ends at the next keyword ("*") card.

VARIABLE DESCRIPTION

Remarks:

1. This boundary condition should only be imposed on a CESE mesh boundary that is in contact with non-moving structural parts. An Eulerian CESE solver is required, as is use of the structural thermal solver.

*CESE_BOUNDARY_CYCLIC_OPTION

Available options are:

MSURF

MSURF_SET

SET

SEGMENT

Purpose: Define a cyclic (periodic) boundary condition for CESE compressible flows. This cyclic boundary condition (CBC) can be used on periodic boundary surfaces.

The MSURF and MSURF_SET options are used when the CESE mesh has been created using *MESH cards. The SET and SEGMENT cards are used when *ELEMENT_SOLID cards are used to define the CESE mesh.

Card Sets. The following sequence of cards comprises a *single set*. LS-DYNA will continue reading *CESE_BOUNDARY_SOLID_WALL card sets until the next keyword ("*") card is encountered.

Card 1a	1	$\overline{2}$	3	4	5	6	7	8
Variable		MSURFID1 MSURFID2	CYCTYP					
Type								
Default	none	none	$\overline{0}$					
Remarks			1, 2					

Surface Part Card. Card 1 format used when the MSURF keyword option is active.

Surface Part Set Card. Card 1 format used when the MSURF_SET keyword option is active.

Set Card. Card 1 format used when the SET keyword option is active.

Segment Card. Card 1 format used when SEGMENT keyword option is active. Include an additional card for each corresponding pair of segments. This input ends at the next keyword ("*") card.

Rotation Case Card. Additional card for the MSURF, MSURF_SET, and SET options when $CYCTYP = 1$.

Translation Case Card. Additional card for the MSURF, MSURF_SET, and SET options when CYCTYP = 2.

DESCRIPTION

Remarks:

- 1. For the MSURF, MSURF_SET, or SET options with CYCTYP.EQ.0, the code examines the geometry of two faces of the two surfaces in order to determine if the surfaces are approximately parallel (CYCTYP.EQ.2), or related through a rotation (CYCTYP.EQ.1). The geometric parameters required are then computed.
- 2. For the MSURF option, there must be the same number of mesh surface elements in each mesh surface part, and the mesh surface elements in each mesh surface part are then internally ordered in order to match pairwise between the two mesh surface parts.
- 3. For the MSURF_SET option, there must be the same number of mesh surface elements in each mesh surface part set, and the mesh surface elements in each mesh surface part set are then internally ordered in order to match pairwise between the two mesh surface part sets.
- 4. For the SET option, there must be the same number of segments in each set, and the segments in each set are then internally ordered in order to match pairwise between the two sets.

*CESE_BOUNDARY_FSI_OPTION

Available options are:

MSURF

MSURF_SET

SET

SEGMENT

Purpose: Define an FSI boundary condition for the moving mesh CESE compressible flow solver. This card must not be combined with the immersed-boundary method CESE solver, and doing so will result in an error termination condition.

This boundary condition must be applied on a surface of the CESE computational domain that is co-located with surfaces of the outside boundary of the structural mechanics mesh. The nodes of the two meshes will generally not be shared.

The MSURF and MSURF_SET options are used when the CESE mesh has been created using *MESH cards. The SET and SEGMENT cards are used when *ELEMENT_SOLID cards are used to define the CESE mesh.

Surface Part Card. Card 1 format used when the MSURF keyword option is active. Provide as many cards as necessary. This input ends at the next keyword ("*") card.

Surface Part Set Card. Card 1 format used when the MSURF_SET keyword option is active. Provide as many cards as necessary. This input ends at the next keyword ("*") card.

Set Card. Card 1 format used when the SET keyword option is active. Provide as many cards as necessary. This input ends at the next keyword ("*") card.

Segment Cards. Card 1 format used when SEGMENT keyword option is active. Include an additional card for each corresponding pair of segments. This input ends at the next keyword ("*") card.

VARIABLE DESCRIPTION

MSURFID Mesh surface part ID referenced in *MESH_SURFACE_ELE-MENT cards.

Remarks:

1. This boundary condition card is also needed for conjugate heat transfer problems with the moving mesh CESE solver.

*CESE_BOUNDARY_NON_REFLECTIVE_OPTION

Available options are:

MSURF MSURF_SET

SET

SEGMENT

Purpose: Define a passive boundary condition for CESE compressible flows. This nonreflective boundary condition (NBC) provides an artificial computational boundary for an open boundary that is passive.

The MSURF and MSURF_SET options are used when the CESE mesh has been created using *MESH cards. The SET and SEGMENT cards are used when *ELEMENT_SOLID cards are used to define the CESE mesh.

Surface Part Card. Card 1 used when the MSURF keyword option is active. Include as many cards as necessary. This input ends at the next keyword ("*") card.

Surface Part Set Card. Card 1 used when the MSURF_SET keyword option is active. Include as many cards as necessary. This input ends at the next keyword ("*") card.

Set Card. Card 1 used when the SET keyword option is active. Include as many cards as necessary. This input ends at the next keyword ("*") card.

Card 1c		$\overline{2}$	3	4	5	6	8
Variable	SSID						
Type							
Default	none						

Segment Cards. Card 1 used when SEGMENT keyword option is active. Include an additional card for each corresponding pair of segments. This input ends at the next keyword ("*") card.

VARIABLE DESCRIPTION

Remarks:

1. This boundary condition is usually imposed on an open surface that is far from the main disturbed flow (the further away, the better), i.e., the flow on that boundary surface should be almost uniform.

2. If any boundary segment has not been assigned a boundary condition by any of the *CESE_BOUNDARY_… cards, then it will automatically be assigned this non-reflective boundary condition.

*CESE_BOUNDARY_PRESCRIBED_OPTION

Available options include:

MSURF MSURF_SET SET

SEGMENT

Purpose: For the CESE compressible flow solver, set boundary values for velocity, density, pressure and temperature. Boundary values are applied at the centroid of elements connected with this boundary. OPTION = SET and OPTION = SEGMENT are for user defined meshes whereas OPTION = MSURF or MSURF_SET are associated with the automatic volume mesher (See *MESH keywords).

That is, the MSURF and MSURF_SET options are used when the CESE mesh has been created using *MESH cards. The SET and SEGMENT cards are used when *ELE-MENT SOLID cards are used to define the CESE mesh.

Card Sets:

A set of data cards for this keyword consists of 3 of the following cards:

- 1. Card 1 specifies the object to which the boundary condition is applied. Its format depends on the keyword option.
- 2. Card 2 reads in load curve IDs.
- 3. Card 3 reads in scale factors.

For each boundary condition to be specified include one set of cards. This input ends at the next keyword ("*") card.

Card 1a		\overline{c}	3	4	5	6	8
Variable	MSURFID	IDCOMP					
Type							
Default	none	none					

Surface Part Card. Card 1 format used when the MSURF keyword option is active.

Surface Part Set Card. Card 1 format used when the MSURF_SET keyword option is active.

Set Card. Card 1 format used when the SET keyword option is active.

Segment Card. Card 1 for SEGMENT keyword option is active.

*CESE_BOUNDARY_PRESCRIBED *CESE

Load Curve Card.

Scale Factor Card.

VARIABLE DESCRIPTION

Remarks:

- 1. On each centroid or set of centroids, the variables (v_x , v_y , v_z , ρ , P , T) that are given values must be consistent and make the model well-posed (i.e., be such that the solution of the model exists, is unique and physical).
- 2. If any of the load curves are 0, the corresponding variable will take the constant value of the corresponding scale factor. For instance, if $LC_RHO = 0$, then the constant value of the density for this boundary condition will be SF_- RHO.
- 3. If a load ID is -1 for a given variable, then the boundary value for that variable is computed by the solver, and not specified by the user.

*CESE_BOUNDARY_PRESCRIBED_VN_OPTION

Available options include:

MSURF MSURF_SET SET

SEGMENT

Purpose: For the CESE compressible flow solver, set boundary values for velocity, density, pressure and temperature. Boundary values are applied at the centroid of elements connected with this boundary. OPTION = SET and OPTION = SEGMENT are for user defined meshes whereas OPTION = MSURF or MSURF_SET are associated with the automatic volume mesher (See *MESH keywords).

That is, the MSURF and MSURF_SET options are used when the CESE mesh has been created using *MESH cards. The SET and SEGMENT cards are used when *ELE-MENT SOLID cards are used to define the CESE mesh.

Card Sets:

A set of data cards for this keyword consists of 3 of the following cards:

- 1. Card 1 specifies the object to which the boundary condition is applied. Its format depends on the keyword option.
- 2. Card 2 reads in load curve IDs.
- 3. Card 3 reads in scale factors.

For each boundary condition to be specified include one set of cards. This input ends at the next keyword ("*") card.

Card 1a		$\overline{2}$	3	4	5	6	8
Variable	MSURFID	IDCOMP					
Type							
Default	none	none					

Surface Part Card. Card 1 format used when the MSURF keyword option is active.

Surface Part Set Card. Card 1 format used when the MSURF_SET keyword option is active.

Set Card. Card 1 format used when the SET keyword option is active.

Segment Card. Card 1 for SEGMENT keyword option is active.

Load Curve Card.

Scale Factor Card.

VARIABLE DESCRIPTION

Remarks:

- 1. On each centroid or set of centroids, the variables (V_N , ρ , P , T) that are given values must be consistent and make the model well-posed (i.e., be such that the solution of the model exists, is unique and physical).
- 2. If any of the load curves are 0, the corresponding variable will take the constant value of the corresponding scale factor. For instance, if $LC_RHO = 0$, then the constant value of the density for this boundary condition will be SF_- RHO.
- 3. If a load ID is -1 for a given variable, then the boundary value for that variable is computed by the solver, and not specified by the user.

*CESE_BOUNDARY_REFLECTIVE_OPTION

Available options are:

MSURF MSURF_SET SET

SEGMENT

Purpose: Define a reflective boundary condition (RBC) for the CESE compressible flow solver. This boundary condition can be applied on a symmetrical surface or a solid wall of the computational domain.

The MSURF and MSURF_SET options are used when the CESE mesh has been created using *MESH cards. The SET and SEGMENT cards are used when *ELEMENT_SOLID cards are used to define the CESE mesh.

Surface Part Card. Card 1 format used when the MSURF keyword option is active. Provide as many cards as necessary. This input ends at the next keyword ("*") card.

Surface Part Set Card. Card 1 format used when the MSURF_SET keyword option is active. Provide as many cards as necessary. This input ends at the next keyword ("*") card.

Set Card. Card 1 format used when the SET keyword option is active. Provide as many cards as necessary. This input ends at the next keyword ("*") card.

Card 1c		$\overline{2}$	3	4	5	6	8
Variable	SSID						
Type							
Default	none						

Segment Cards. Card 1 format used when SEGMENT keyword option is active. Include an additional card for each corresponding pair of segments. This input ends at the next keyword ("*") card.

- MSURFID Mesh surface part ID referenced in *MESH_SURFACE_ELE-MENT cards.
- MSURF_{_S} Identifier of a set of mesh surface part IDs created with a *LSO_{_}-ID_SET card, where each mesh surface part ID in the set is referenced in *MESH_SURFACE_ELEMENT cards.
- SSID Segment set ID.
- N1, N2, ... Node IDs defining a segment

Remarks:

1. This boundary condition has the same effect as a solid-wall boundary condition for inviscid flows.

*CESE_BOUNDARY_SLIDING_OPTION

Available options are:

MSURF

MSURF_SET

SET

SEGMENT

Purpose: Allows nodes of a fluid surface to translate in the main direction of mesh movement. This is useful in piston type applications.

The MSURF and MSURF_SET options are used when the CESE mesh has been created using *MESH cards. The SET and SEGMENT cards are used when *ELEMENT_SOLID cards are used to define the CESE mesh.

Surface Part Card. Card 1 format used when the MSURF keyword option is active. Provide as many cards as necessary. This input ends at the next keyword ("*") card.

Surface Part Set Card. Card 1 format used when the MSURF_SET keyword option is active. Provide as many cards as necessary. This input ends at the next keyword ("*") card.

Set Card. Card 1 format used when the SET keyword option is active. Provide as many cards as necessary. This input ends at the next keyword ("*") card.

Segment Cards. Card 1 format used when SEGMENT keyword option is active. Include an additional card for each corresponding pair of segments. This input ends at the next keyword ("*") card.

VARIABLE DESCRIPTION

N1, N2, ... Node IDs defining a segment

*CESE_BOUNDARY_SOLID_WALL_OPTION1_OPTION2

For *OPTION1* the choices are:

MSURF

MSURF_SET

SET

SEGMENT

For *OPTION2* the choices are:

<BLANK>

ROTAT

Purpose: Define a solid wall boundary condition (SBC) for this CESE compressible flow solver. This boundary condition can be applied at a solid boundary that is the physical boundary for the flow field. For inviscid flow, this will be a slip boundary condition; while for viscous flows, it is a no-slip boundary condition.

The MSURF and MSURF_SET options are used when the CESE mesh has been created using *MESH cards. The SET and SEGMENT cards are used when *ELEMENT_SOLID cards are used to define the CESE mesh.

Card Sets. The following sequence of cards comprises a *single set*. LS-DYNA will continue reading *CESE_BOUNDARY_SOLID_WALL card sets until the next keyword ("*") card is encountered.

Surface Part Card. Card 1 format used when the MSURF keyword option is active.

Surface Part Set Card. Card 1 format used when the MSURF_SET keyword option is active.

Set Card. Card 1 format used when the SET keyword option is active.

Segment Card. Card 1 format used when SEGMENT keyword option is active.

Rotating Axis Card. Additional card for the "Segment Card" case that is read when the ROTAT keyword option is used.

LCID.NE.0: it will be defined by both of the load curve and (Vx, Vy, Vz); Nx, Ny, Nz are not used in this case.

If OPTION2 = ROTAT:

Remarks:

- 1. In this solid-wall condition (SBC), the boundary movement can only be in the tangential direction of the wall and should not affect the fluid domain size and mesh during the calculation, otherwise an FSI or moving mesh solver should be used. Also, this moving SBC only affects viscous flows (no-slip BC).
- 2. If LCID = 0 and $Vx = Vy = Vz = 0.0$ (default), this will be a regular solid wall BC.
- 3. For rotating SBC, LCID > 0 must be used to define the rotating speed frequency (Hz). Also, in the 2D case, (Nx, Ny, Nz) does not need to be defined because it is not needed.

*CESE_CHEMISTRY_**D3**PLOT

Purpose: Cause mass fractions of the listed chemical species to be added to the CESE d3plot output. This is only used when chemistry is being solved with the CESE solver.

Species Cards. Include one card for each species to be included in the d3plot database. This input ends at the next keyword ("*") card.

VARIABLE DESCRIPTION

MODELID Identifier of a Chemkin-compatible chemistry model.

SPECIES Name of a chemical species that is defined in the chemistry model identified by MODELID (see *CHEMISTRY_MODEL).

*CESE_CONTROL_LIMITER

Purpose: Sets some stability parameters used in the CESE scheme for this CESE compressible flow solver.

Remarks:

- 1. $\alpha \geq 0$; larger values give more stability, but less accuracy. Usually $\alpha = 2.0$ or 4.0 will be enough for normal shock problems.
- 2. $0 \le \beta \le 1$; larger values give more stability. For problems with shock waves, β = 1.0 is recommended.
- 3. $\varepsilon \geq 0$; larger values give more stability, but less accuracy.

*CESE_CONTROL_MESH_MOV

Purpose: For moving mesh CESE, this keyword is used to choose the type of algorithm to be used for calculating mesh movement.

.

*CESE_CONTROL_SOLVER

Purpose: Set general purpose control variables for the CESE compressible flow solver.

Remarks:

- 1. If the user wants to use the 2D (IGEOM = 2) or 2D axisymmetric (IGE- $OM = 101$) solver, the mesh should only be distributed in the x-y plane with the boundary conditions given only at the $x-y$ domain boundaries. Otherwise, a warning message will be given and the 3D solver will be triggered instead.
- 2. The 2D axisymmetric case will work only if the 2D mesh and corresponding boundary conditions are properly defined, with the x and y coordinates corresponding to the radial and axial directions respectively.
- 3. IDC is the same type of variable that is input on the *ICFD_CONTROL_FSI card. For an explanation, see Remark 1 for the *ICFD_CONTROL_FSI card.

*CESE_CONTROL_TIMESTEP

Purpose: Sets the time-step control parameters for the CESE compressible flow solver.

VARIABLE DESCRIPTION

*CESE_DATABASE_**ELOUT**

Purpose: This keyword enables the output of CESE data on elements. If more than one element set is defined, then several output files will be generated.

Output Options Card.

Include as many cards as needed. This input ends at the next keyword ("*") card.

Remarks:

1. The file name for this database is cese_elout.dat.

*CESE_DATABASE_**FLUXAVG**

Purpose: This keyword enables the output of CESE data on segment sets. If more than one segment set is defined, then several output files will be generated.

Output Options Card.

Include as many cards as needed. This input ends at the next keyword ("*") card.

Remarks:

1. The file names for this database is cese_fluxavg.dat.
*CESE_DATABASE_**FSIDRAG**

Purpose: This keyword enables the output of the total fluid pressure force applied on solid parts in FSI problems at every time step.

Output Options Card.

VARIABLE DESCRIPTION

OUTLV Determines if the output file should be dumped.

EQ.0: No output file is generated.

EQ.1: The output file giving the pressure forces is generated.

Remarks:

1. The file names for this database are cese_dragsol.dat*,* cese_dragshell.dat*,* cese_dragsol2D.dat and cese_dragbeam.dat .depending on what kind of solid is used.

*CESE_DATABASE_**POINTOUT**

Purpose: This keyword enables the output of CESE data on points.

Output Options Card.

Include as many cards as needed. This input ends at the next keyword ("*") card.

Remarks:

1. The file name for this database is cese_pointout.dat.

*CESE_DATABASE_**SSETDRAG**

Purpose: This keyword enables the output of CESE drag forces on segment sets. If more than one segment set is defined, then several output files will be generated.

Output Options Card.

Include as many cards as needed. This input ends at the next keyword ("*") card.

Remarks:

1. The file name for this database is *cese_ssetdrag.dat*.

2. In order for the friction drag to give consistent results, special care must be given to the mesh close to the solid wall boundary (Good capturing of the boundary layer behavior). A very fine structured mesh is recommended.

*CESE_**DEFINE_NONINERTIAL**

Purpose: Define the CESE problem domain as a non-inertial rotating frame that rotates at a constant rate. This is used in rotating problems such as spinning cylinders, wind turbines and turbo machinery.

VARIABLE DESCRIPTION

VARIABLE DESCRIPTION RELV Velocity display mode: EQ.0: Relative velocity, only the non-rotating components of

the velocity are output. EQ.1: Absolute velocity is output.

*CESE_DEFINE_**POINT**

Purpose: Define points to be used by the CESE solver.

Point Cards. Include one card for each point. This input ends at the next keyword $($ "*") card.

VARIABLE DESCRIPTION

- NID Identifier for this point.
- X, Y, Z Coordinates of the point.

*CESE_**DRAG**

Purpose: Provide the far-field (or free-stream) fluid pressure.

VARIABLE DESCRIPTION

PRESS Value of the free-stream fluid pressure (in units used by the current problem).

*CESE_EOS_CAV_HOMOG_EQUILIB

Purpose: Define the coefficients in the equation of state (EOS) for the homogeneous equilibrium cavitation model.

Include as many cards as needed. This input ends at the next keyword ("*") card.

Remarks:

- 1. Once a cavitation EOS is used, the cavitation flow solver will be triggered.
- 2. In this homogeneous equilibrium cavitation model, a barotropic equation of state is used. This model can be used in small scale & high speed cavitation flows, and it is not good for large-scale, low-speed cavitation calculations.

*CESE_EOS_IDEAL_GAS

Purpose: Define the coefficients Cv and Cp in the equation of state for an ideal gas in the CESE fluid solver.

VARIABLE DESCRIPTION

- EOSID Equation of state identifier
	- Cv Specific heat at constant volume
	- Cp Specific heat at constant pressure

Remarks:

1. **Units.** As with other solvers in LS-DYNA, the user is responsible for unit consistency. For example, if a user wants to use dimensionless variables, Cv and Cp should also be replaced by the corresponding dimensionless ones.

*CESE_EOS_INFLATOR1

Purpose: To define an EOS using Cp and Cv thermodynamic expansions for an inflator gas mixture with a single temperature range.

VARIABLE DESCRIPTION

EOSID Equation of state identifier for the CESE solver.

Cp0, …, Cp4 Coefficients of temperature-dependent specific heat at constant pressure

 $C_p(T) = C_{p0} + C_{p1} T + C_{p2} T^2 + C_{p3} T^3 + C_{p4} T^4$

VARIABLE DESCRIPTION

Cv0, …, Cv4 Coefficients of temperature-dependent specific heat at constant volume

 $C_v(T) = C_{v0} + C_{v1} T + C_{v2} T^2 + C_{v3} T^3 + C_{v4} T^4$

Remark:

1.These coefficient expansions for the specific heats over the entire temperature range are generated by the 0-D inflator model solver. See *CHEMISTRY_CON-TROL_INFLATOR and *CHEMISTRY_INFLATOR_PROPERTIES for details related to running that solver.

*CESE_EOS_INFLATOR2

Purpose: To define an EOS using Cp and Cv thermodynamic expansions for an inflator gas mixture with two temperature ranges, one below 1000 degrees Kelvin, and the other above 1000 degrees Kelvin.

Card for the expansion of Specific Heat at Constant Pressure. Valid for T < $1000\text{ }^{\circ}\text{K}$

Card for the expansion of Specific Heat at Constant Pressure. Valid for $T > 1000 \degree K$.

*CESE_EOS_INFLATOR2 *CESE

Card 4		$\overline{2}$	3	4	5	6	8
Variable	$Cv1_0$	$Cv1_1$	$Cv1_2$	$Cv1_3$	$Cv1_4$		
Type	F	F	F	F	F		
Default	0.	0.	0.	0.	0.		

Card for the expansion of Specific Heat at Constant Volume. Valid for T < 1000 $\mathrm{^0 K}$

Card for the expansion of Specific Heat at Constant Volume. Valid for $T > 1000 \degree K$.

Remark:

2.These coefficient expansions for the specific heats over two temperature ranges are generated by the 0-D inflator model solver. See *CHEMISTRY_CONTROL_IN-FLATOR and *CHEMISTRY_INFLATOR_PROPERTIES for details related to running that solver.

*CESE_**FSI_EXCLUDE**

Purpose: Provide a list of mechanics solver parts that are not involve in the CESE FSI calculation. This is intended to be used as an efficiency measure for parts that will not involve significant FSI interactions with the CESE compressible fluid solver..

Include as many cards as needed. This input ends at the next keyword ("*") card.

VARIABLE DESCRIPTION

PIDn IDs of mechanics parts that will be excluded from the FSI interaction calculation with the CESE solver.

*CESE_INITIAL

Purpose: Specify constant initial conditions (ICs) for flow variables at the centroid of each fluid element.

DESCRIPTION

U, V, W x -, y -, z -velocity components, respectively RHO Density, ρ P Pressure, P T Temperature, T

Remarks:

- 1. **Required Input.** Usually, only two of ρ , P , and T need to be specified (besides the velocity). If all three are given, only ρ and P will be used.
- 2. **Applicable Elements.** These initial conditions will be applied only in those elements that have not been assigned a value by *CESE_INITIAL_*OPTION* cards for individual elements or sets of elements.

*CESE_INITIAL_OPTION

Available options include:

SET

ELEMENT

Purpose: Specify initial conditions for the flow variables at the centroid of each element in a set of elements or at the centroid of a single element.

Include as many cards as needed. This input ends at the next keyword ("*") card.

Remarks:

- **1.** Required Input. Usually, only two of ρ , P , and T need to be specified (along with the velocity). If all three are given, only ρ and P will be used.
- 2. Initial Condition Specification Priority. The priority of this card is higher than *CESE_INITIAL, meaning that if an element is assigned an initial value by this card, *CESE_INITIAL will no longer apply to that element.

*CESE_INITIAL_CHEMISTRY

Purpose: Initializes the chemistry and fluid state in every element of the CESE mesh that has not already been initialized by one of the other *CESE_INITIAL_CHEMISTRY cards. This is only used when chemistry is being solved with the CESE solver.

VARIABLE DESCRIPTION

- CHEMID Identifier of chemistry control card to use
- COMPID Identifier of chemical composition to use
	- UIC X-component of the fluid velocity
	- VIC Y-component of the fluid velocity
	- WIC Z-component of the fluid velocity
- RHOIC Initial fluid density
- PIC Initial fluid pressure
- TIC Initial fluid temperature

VARIABLE DESCRIPTION

HIC Initial fluid enthalpy. However, when CHEMID refers to a ZND 1-step reaction card, this is the progressive variable (degree of combustion).

*CESE_INITIAL_CHEMISTRY_ELEMENT

Purpose: Initializes the chemistry and fluid state in every element of the list of CESE elements. This is only used when chemistry is being solved with the CESE solver.

Element List Card. Include as many cards as necessary. This input ends at the next keyword ("*") card.

*CESE_INITIAL_CHEMISTRY_ELEMENT *CESE

*CESE_INITIAL_CHEMISTRY_PART

Purpose: Initializes the chemistry and fluid state in every element of the specified CESE part that has not already been initialized by *CESE_INITIAL_CHEMISTRY_ELEMENT or *CESE_INITIAL_CHEMISTRY_SET cards. This is only used when chemistry is being solved with the CESE solver.

HIC Initial fluid enthalpy. However, when CHEMID refers to a ZND 1-step reaction card, this is the progressive variable (degree of combustion).

*CESE_INITIAL_CHEMISTRY_SET

Purpose: Initializes the chemistry and fluid state in every element of the specified element set in the CESE mesh that has not already been initialized by *CESE_INITIAL_**-** CHEMISTRY_ELEMENT cards. This is only used when chemistry is being solved with the CESE solver.

VARIABLE DESCRIPTION

HIC Initial fluid enthalpy. However, when CHEMID refers to a ZND 1-step reaction card, this is the progressive variable (degree of combustion).

*CESE_MAT_000

Purpose: Define the fluid (gas) properties in a viscous flow for the CESE solver.

Material Definition Cards. Include one card for each instance of this material type. This input ends at the next keyword ("*") card.

VARIABLE DESCRIPTION

Remarks:

- 1. The viscosity is only used viscous flows, so for inviscid flows, it is not necessary to define it. The thermal conductivity is only used to calculate the heat transfer between the structure and the thermal solver when coupling is activated.
- 2. As with other solvers in LS-DYNA, the user is responsible for unit consistency. For example, if dimensionless variables are used, MU should be replaced by the corresponding dimensionless one.

*CESE_MAT_001(_GAS)

Purpose: Define the fluid (gas) properties in a viscous flow for the CESE solver.

Include as many cards as needed. This input ends at the next keyword ("*") card.

VARIABLE DESCRIPTION

- MID Material identifier
- C1, C2 Two coefficients in the Sutherland's formula for viscosity, i.e.,

$$
\mu=\frac{C_1T^{\frac{3}{2}}}{T+C_2}
$$

where C_1 and C_2 are constants for a given gas. For example, for air at moderate temperatures,

 $C_1 = 1.458 \times 10^{-6}$ kg/msK^{1/2}, $C_2 = 110.4$ K

PRND The Prandtl Number (used to determine the coefficient of thermal conductivity). It is approximately constant for most gases. For air at standard conditions $PRND = 0.72$.

Remarks:

- 1. C1 and C2 are only used to calculate the viscosity in viscous flows, so for inviscid flows, this material card is not needed. The Prandtl number is used to extract the thermal conductivity, which is used when thermal coupling with the structure is activated.
- 2. As with other solvers in LS-DYNA, the user is responsible for unit consistency. For example, if dimensionless variables are used, C_1 and C_2 should be replaced by the corresponding dimensionless ones.

*CESE_MAT_002

Purpose: Define the fluid (gas) properties in a viscous flow for the CESE solver.

Material Definition Cards. Include one card for each instance of this material type. This input ends at the next keyword ("*") card.

VARIABLE DESCRIPTION

MID Material identifier

MU0 / SMU Two coefficients appearing in the equation derived by combining Sutherland's formula with the power law for dilute gases:

$$
\frac{\mu}{\mu_0} = \left(\frac{T}{T_0}\right)^{3/2} \frac{T_0+S_\mu}{T+S_\mu}~.
$$

 μ_0 is a reference value, and S_u is an effective temperature called the Sutherland constant, which is characteristic of the gas. For air at moderate temperatures,

$$
\mu_0 = 1.716 \times 10^{-5} \text{Ns/m}^2
$$
, $S_\mu = 111 \text{ K}$

K0/SK Two coefficients appearing in the equation derived by combining Sutherland's formula with the power law for dilute gases:

$$
\frac{k}{k_0} = \left(\frac{T}{T_0}\right)^{3/2} \frac{T_0+S_k}{T+S_k} \ .
$$

Here *k* is the thermal conductivity, k_0 is a reference value, and S_k is the Sutherland constant, which is characteristic of the gas. For air at moderate temperatures,

$$
k_0 = 0.0241 \, \text{W/m}, \qquad S_k = 194 \, \text{K}
$$

T0 Reference temperature, T_0 . The default value (273.0) is for air, in degrees K.

Remarks:

- 1. Fields that Depend on Problem Physics. The viscosity is only used for viscous flow. Therefore, for inviscid flows, it is not necessary to define it. The thermal conductivity is only used to calculate the heat transfer between the structure and the thermal solver when coupling is activated.
- 2. **Unit Consistency.** As with other solvers in LS-DYNA, the user is responsible for unit consistency. For example, if dimensionless variables are used, MU should be replaced by the corresponding dimensionless one.

*CESE_PART

Purpose: Define CESE solver parts, i.e., connect CESE material and EOS information.

Part Cards. Include one card for each CESE part. This input ends at the next keyword $($ "*") card.

Card 1		$\overline{2}$	3	4	5	6	8
Variable	PID	MID	EOSID				
Type							
Default	none	none	none				

Remarks:

1. Since material coefficients are only used in viscous flows, the MID can be left blank for inviscid flows.

*CESE_**SURFACE_MECHSSID_D3PLOT**

Purpose: Identify the surfaces to be used in generating surface D3PLOT output for the CESE solver. These surfaces must be on the outside of volume element parts that are in contact with the CESE fluid mesh. The variables in question are part of the CESE FSI solution process or of the CESE conjugate heat transfer solver.

Include as many cards as needed. This input ends at the next keyword ("*") card.

*CESE_**SURFACE_MECHVARS_D3PLOT**

Purpose: List of variables to output on the surfaces designated by the segment set IDs given in the *CESE_SURFACE_MECHSSID_D3PLOT cards. Most of the allowed variables are defined only on the fluid-structure interface, and so the segment set IDs defining a portion of the fluid-structure interface must involve only segments (element faces) that are on the outside of volume element parts that are in contact with the CESE fluid mesh.

Include as many cards as needed. This input ends at the next keyword ("*") card.

VARIABLE DESCRIPTION

Output Quantity

VARIABLE DESCRIPTION

Descriptive phrase for the mechanics surface variable to output for the LSPP user. Output will be done on all SSIDs selected by the *CESE_SURFACE_MECHSSID_D3PLOT cards in the problem.

Supported variables include:

FLUID FSI FORCE FLUID FSI PRESSURE INTERFACE TEMPERATURE SOLID INTERFACE HEAT FLUX FLUID INTERFACE HEAT FLUX INTERFACE HEAT FLUX RATE SOLID INTERFACE DISPLACEMENT SOLID INTERFACE VELOCITY SOLID INTERFACE ACCELERATION

Force, displacement, velocity, and acceleration are output as vector quantities. The rest of the variables are scalar quantities. The fluxes are in the normal direction to the fluid/structure interface, with the heat fluxes relative to the normal pointing into the structure.
*CHEMISTRY

The keyword *CHEMISTRY is used to access chemistry databases that include Chemkin-based descriptions of a chemical model, as well as to select a method of solving the model. The keyword cards in this section are defined in alphabetical order:

*CHEMISTRY_BLAST_INITIATION

*CHEMISTRY_COMPOSITION

*CHEMISTRY_CONTROL_0D

*CHEMISTRY_CONTROL_1D^T

*CHEMISTRY_CONTROL_CSP

*CHEMISTRY_CONTROL_FULL

*CHEMISTRY_CONTROL_INFLATOR†

*CHEMISTRY_CONTROL_TBX

*CHEMISTRY_CONTROL_ZND†

*CHEMISTRY_DET_INITIATION†

*CHEMISTRY_INFLATOR_PROPERTIES†

*CHEMISTRY_MODEL

*CHEMISTRY_PATH

†: Card may be used only once in a given model

An additional option **"_**TITLE**"** may be appended to all *CHEMISTRY keywords. If this option is used, then an 80 character string is read as a title from the first card of that keyword's input. At present, LS-DYNA does not make use of the title. Inclusion of titles gives greater clarity to input decks.

In order to use one of the chemistry solvers, the input must include at least one *CHEM-ISTRY_MODEL card. For each spatial region containing a different chemical composition, at least one *CHEMISTRY_COMPOSITION card is required.

*CHEMISTRY

The *CHEMISTRY_CONTROL_0D card is intended to be used in a standalone fashion to verify the validity of a given chemistry model. This model includes the total number of species and all elementary reactions with their Arrhenius rate parameters. For instance, this solver could be used to check the induction time of the model.

The *CHEMISTRY_BLAST_INITIATION, *CHEMISTRY_CONTROL_1D, *CHEM-ISTRY_DET_INITIATION, and *CHEMISTRY_CONTROL_ZND cards are intended to provide a one-dimensional initialization to a 2D or 3D chemically-reacting flow.

In order to perform a full, general purpose chemistry calculation in 2D or 3D, the *CHEMISTRY_CONTROL_FULL card should be used.

The *CHEMISTRY_CONTROL_CSP card is an option for reducing the number of species and reactions that are used in a general purpose chemistry calculation. Other reduction mechanisms are planned for the future.

An airbag inflator model is available with *CHEMISTRY_CONTROL_INFLATOR along with *CHEMISTRY_INFLATOR_PROPERTIES and a chemistry model that is referenced via three chemical compositions. This involves zero-dimensional modeling, with pyrotechnic inflator, and cold and hot flow hybrid inflator options.

The *CHEMISTRY_CONTROL_TBX card is intended for use only in a stochastic particle model, where the *STOCHASTIC_TBX_PARTICLES card is used.

*CHEMISTRY_COMPOSITION

Purpose: Provides a general way to specify a chemical composition via a list of species mole numbers in the context of a Chemkin database model.

Species List Card. Provide as many cards as necessary. This input ends at the next keyword ("*") card.

*CHEMISTRY_CONTROL_0D

Purpose: Performs a zero-dimensional isotropic chemistry calculation that operates standalone (does not call the CESE solver). This is for ISOBARIC or ISOCHORIC cases.

CSP Parameters Card. Include cards for each chemical species in the following format when CSP_SEL.GT.0. This input ends at the next keyword ("*") card.

VARIABLE DESCRIPTION

ID Identifier for this 0D computation.

Remarks:

1. If CSP_SEL.GT.0, then instead of using the full chemistry solver, the computational singular perturbation (CSP) method solver is used.

*CHEMISTRY_CONTROL_1D

Purpose: Loads a previously-computed one-dimensional detonation. It is then available for use in the CESE solver for initializing a computation. In the product regions, this card overrides the initialization of the *CESE_INITIAL_CHEMISTRY_… cards.

One-Dimensional Solution LSDA Input File Card.

CSP Parameters Card Include cards for each chemical species in the following format when CSP_SEL > 0. This input ends at the next keyword ("*") card.

VARIABLE DESCRIPTION

ID Identifier for this one-dimensional detonation solution.

Remarks:

1. If CSP_SEL > 0, then instead of using the full chemistry solver, the computational singular perturbation (CSP) method solver is used.

*CHEMISTRY_CONTROL_CSP

Purpose: Computes reduced chemistry for a specified Chemkin chemistry model using the Computational Singular Perturbation (CSP) method. This card can be used for general-purpose chemical reaction calculations.

CSP Parameters Card. Include cards for each chemical species in the following format as indicated by the value of IERROPT. This input ends at the next keyword ("*") card.

DESCRIPTION

*CHEMISTRY_CONTROL_FULL

Purpose: Computes the full chemistry specified by a Chemkin chemistry model. This card can be used for general-purpose chemical reaction calculations.

*CHEMISTRY_**CONTROL_INFLATOR**

Purpose: Provide the required properties of an inflator model for airbag inflation.

Inflator Output Database File (an ASCII file) Card.

Densities for Condensed Species. Include as many cards as needed. This input ends at the next keyword ("*") card.

VARIABLE DESCRIPTION

4-10 (CHEMISTRY) LS-DYNA R12

*CHEMISTRY_**CONTROL_INFLATOR** *CHEMISTRY

Remarks:

1. If MODEL = 3, the solution of an elementary reaction system is required for the finite-rate chemistry in the gas chamber. For $MODEL = 4$ and 5, the condensed phase is computed only in the combustion chamber.

- 2. Output file includes all of the necessary thermodynamics variables and load curves for the species mass flow rate, temperature, and density curve. This will make it possible to generate the velocity curve which is required by each solver that carries out an airbag simulation.
- 3. At least one of these cards will be input if condensed-phase species are present during the propellant combustion. In this case, the user must specify each condensed-phase density. This density is then used to compute the volume fractions in both the combustion and gas chamber, where the energy equations are needed.
- 4. If OUT_TYPE = 0, the propellant information will be displayed on the screen, including total mass, remaining mass percentage, and mass burning rate versus time, and the calibration data will be saved in the output file, including the time versus pressure, temperature, total mass flow rate, and individual species mass fractions for all chambers. With this option, the user can quickly see the effect of changing the parameters on the first three *CHEMISTRY_INFLA-TOR_PROPERTIES cards.

*CHEMISTRY_**CONTROL_TBX**

Purpose: Specify a chemistry solver for use in conjunction with stochastic TBX particles. This is intended only for modeling the second phase of an explosion where the explosive has embedded metal (aluminum) particles that are too large to have burned in the first phase of the explosion.

This chemistry card points to a *CHEMISTRY_MODEL card (via IDCHEM) with its associated *CHEMISTRY_COMPOSITION cards to set up the initial conditions. That is, it establishes the spatial distribution of the species in the model.

It is assumed that there is no chemical reaction rate information in the chemistry model files. This is done since a special chemical reaction mechanism is implemented for TBX modeling. If particles other than solid aluminum particles are embedded in the explosive, then another burn model has to be implemented.

Surface Part Card. Card 1 format used when the PART keyword option is active.

*CHEMISTRY_CONTROL_ZND

Purpose: Computes the one-dimensional reduced chemistry of a ZND model. It is then used in the initialization of the chemistry part of the CESE solver. When this card is used, the *CESE_INITIAL_CHEMISTRY… cards must specify the progressive variable (degree of combustion) in the HIC field.

*CHEMISTRY_DET_INITIATION

Purpose: Performs a one-dimensional detonation calculation based upon a chemical composition and initial conditions. It is then available for use immediately in the CESE solver for initializing a computation, or it can be subsequently used by the *CHEM-ISTRY_CONTROL_1D card in a later run. In the product regions, this card overrides the initialization of the *CESE_INITIAL_CHEMISTRY… cards.

LSDA Output File Card.

VARIABLE DESCRIPTION

FILE Name of the LSDA file in which to write the one-dimensional solution.

*CHEMISTRY_**INFLATOR_PROPERTIES**

Purpose: Provide the required properties of an inflator model.

Combustion Chamber Parameter Card.

Gas Plenum Parameter Card.

Tank Parameter Card.

Type | I | F | F | F | F | F | F | F

Default | none | none | none | none | none | none | none

*CHEMISTRY_**INFLATOR_PROPERTIES** *CHEMISTRY

Gas Chamber 2 (Optional, see Remark 3) Card.

Remarks:

- 1. The propellant composition can be obtained by running a chemical equilibrium program such as NASA CEA, the CHEETAH code, or the PEP code. LSTC provides a modified version of the PEP code along with documentation for users; it is available upon request.
- 2. A spherical shape for the propellant particles can be chosen if an identical value for the diameter and height is given.
- 3. To simulate a 4 or 5 chamber inflator, an additional chamber card can be used. In these cases of the inflator models, the condensed phase species are limited to the combustion chamber only if involved in the propellant combustion.

*CHEMISTRY_**MODEL**

Purpose: Identifies the files that define a Chemkin chemistry model.

Chemkin Input File Card.

Thermodynamics Database File Card.

Transport Properties Database File Card.

VARIABLE DESCRIPTION

MODELID Identifier for this Chemkin-based chemistry model..

*CHEMISTRY *CHEMISTRY_PATH

*CHEMISTRY_PATH

Purpose: To specify one or more search paths to look for chemistry database files.

Include as many cards as needed. This input ends at the next keyword ("*") card.

VARIABLE DESCRIPTION

DIR Directory path to add to the search set.

*DUALCESE

The keyword *DUALCESE provides input data for the dual Conservation Element/Solution Element (dual CESE) compressible fluid solver:

*DUALCESE_BOUNDARY_AXISYMMETRIC_{OPTION}

*DUALCESE_BOUNDARY_FSI_{OPTION}

*DUALCESE_BOUNDARY_NON_REFLECTIVE_{OPTION}

*DUALCESE_BOUNDARY_PRESCRIBED_{OPTION}

*DUALCESE_BOUNDARY_REFLECTIVE_{OPTION}

*DUALCESE_BOUNDARY_SOLID_WALL_{OPTION1}_{OPTION2}

*DUALCESE_CONTROL_LIMITER

*DUALCESE_CONTROL_MESH_MOV

*DUALCESE_CONTROL_SOLVER

*DUALCESE_CONTROL_TIMESTEP

*DUALCESE_D3PLOT

*DUALCESE_D3PLOT_FLUID_SSID

*DUALCESE_ELE2D

*DUALCESE_ELE3D

*DUALCESE_ELEMENTSET

*DUALCESE_EOS_COOLPROP

*DUALCESE_EOS_IDEAL_GAS

*DUALCESE_EOS_INFLATOR1

*DUALCESE_EOS_INFLATOR2

*DUALCESE_EOS_REFPROP

*DUALCESE_EOS_REFPROP_PATH

*DUALCESE_FSI_EXCLUDE

*DUALCESE_INCLUDE_MODEL *DUALCESE_INITIAL *DUALCESE_INITIAL_{OPTION} *DUALCESE_MAT_GAS *DUALCESE_MAT_GAS_0 *DUALCESE_MAT_GAS_2 *DUALCESE_MODEL *DUALCESE_NODE2D *DUALCESE_NODE3D *DUALCESE_NODESET *DUALCESE_PART *DUALCESE_SEGMENTSET

It should be noted that capabilities implemented in the dual CESE solvers are only a part of what is available in the *CESE solvers that involve couplings with the *CHEM-ISTRY and *STOCHASTIC_PARTICLE solvers. It is planned to port many of those capabilities to the *DUALCESE solvers as well.

Another important note concerns the setup of input decks for simulations using *DU-ALCESE capabilities. Since there can be several *DUALCESE models in the same problem, each such model is restricted to be specified with one file hierarchy that starts with the keyword file designated with the *DUALCESE_MODEL card. That keyword file can include any number of other keyword files with the *DUALCESE_INCLUDE_- MODEL card, and each of those files can in turn include other keyword files, again with the *DUALCESE_INCLUDE_MODEL card. Standard *INCLUDE cards are not allowed. In fact, in each file in the file hierarchy of a *DUALCESE_MODEL card, only *DUALCESE cards may be used. A fatal error will be encountered otherwise.

Any required non-*DUALCESE keyword cards should be defined in some other place in the keyword input.

Since use of the REFPROP and COOLPROP equation of state (EOS) libraries is complex, clarification about their use is also required. Each of them is accessed via a shared library that has to be loaded into LS-DYNA at runtime via a *MODULE_LOAD card such as:

*MODULE_LOAD UserA DUALCESE REFPROP <path to the installed REFPROP shared library>

Note that this *MODULE_LOAD card must not be given inside a keyword file in the file hierarchy of a *DUALCESE_MODEL card. As noted above, this is the case for all non- *DUALCESE keyword cards.

Note further that the REFPROP and COOLPROP libraries are not provided by ANSYS. The user needs to purchase REFPROP 9.1 from NIST (www.nist.gov) in order to make use of *DUALCESE_EOS_REFPROP, and then the user is required to build the REF-PROP shared library from the fortran source files provided by NIST.

For the COOLPROP shared library, the user can find the current production version here:

https://sourceforge.net/projects/coolprop/files/CoolProp/6.3.0/shared_library/Linu $x/64$ bit/

As the *DUALCESE capability is not yet working in the Windows build of LS-DYNA, do not attempt to use a Windows DLL version of the REFPROP shared library that comes with purchasing REFPROP 9.1, or download the Windows DLL version of COOLPROP.

*DUALCESE_BOUNDARY_AXISYMMETRIC_OPTION

Available options are

MSURF_SET

SEGMENT_SET

Purpose: Define an axisymmetric boundary condition on the axisymmetric axis for the 2D axisymmetric dual CESE compressible flow solver.

The MSURF_SET option is used when the dual CESE mesh has been created using *MESH cards. The SEGMENT_SET card is used when *DUALCESE_ELE2D or *DUAL-CESE_ELE3D cards are used to define the dual CESE mesh.

Surface Part Set Card. Card 1 format used when the MSURF_SET keyword option is active. Provide as many cards as necessary. This input ends at the next keyword ("*") card.

Segment Set Card. Card 1 format used when the SEGMENT_SET keyword option is active. Provide as many cards as necessary. This input ends at the next keyword ("*") card.

Remarks:

1. This boundary condition can only be used on the axisymmetric axis for the 2D axisymmetric dual CESE fluid solver.

*DUALCESE_BOUNDARY_FSI_OPTION

Available options are:

MSURF_SET

SEGMENT_SET

Purpose: Define an FSI boundary condition for the moving mesh dual CESE compressible flow solver. This card must not be combined with the dual CESE immersed-boundary method (IBM) FSI solver in the same dual CESE part on the same dual CESE mesh. Doing so will result in an error termination condition.

This boundary condition must be applied on a surface of the dual CESE computational domain that is co-located with surfaces of the outside boundary of the structural mechanics mesh. The nodes of the two meshes will generally not be shared.

The MSURF_SET option is used when the dual CESE mesh has been created using *MESH cards. The SEGMENT_SET card is used when *DUALCESE_ELE2D or *DUAL-CESE_ELE3D cards are used to define the dual CESE mesh.

Surface Part Set Card. Card 1 format used when the MSURF_SET keyword option is active. Provide as many cards as necessary. This input ends at the next keyword ("*") card.

Set Card. Card 1 format used when the SET keyword option is active. Provide as many cards as necessary. This input ends at the next keyword ("*") card.

Remarks:

1. This boundary condition card is also needed for conjugate heat transfer problems with the moving mesh dual CESE solver.

*DUALCESE_BOUNDARY_NON_REFLECTIVE_OPTION

Available options are:

MSURF_SET

SEGMENT_SET

Purpose: Define a passive boundary condition for dual CESE compressible flows. This non-reflective boundary condition (NBC) provides an artificial computational boundary for an open boundary that is passive.

The MSURF_SET option is used when the dual CESE mesh has been created using *MESH cards. The SEGMENT_SET card is used when *DUALCESE_ELE2D or *DUAL-CESE ELE3D cards are used to define the dual CESE mesh.

Surface Part Set Card. Card 1 used when the MSURF_SET keyword option is active. Include as many cards as necessary. This input ends at the next keyword ("*") card.

Set Card. Card 1 used when the SET keyword option is active. Include as many cards as necessary. This input ends at the next keyword ("*") card.

VARIABLE DESCRIPTION

Remarks:

- 1. This boundary condition is usually imposed on an open surface that is far from the main disturbed flow (the further away, the better), i.e., the flow on that boundary surface should be almost uniform.
- 2. If any boundary segment has not been assigned a boundary condition by any of the *DUALCESE_BOUNDARY_… cards, then it will automatically be assigned this non-reflective boundary condition.

*DUALCESE_BOUNDARY_PRESCRIBED_OPTION

Available options include:

MSURF_SET

SEGMENT_SET

Purpose: For the dual CESE compressible flow solver, set boundary values for velocity, density, pressure and temperature. Boundary values are applied at the centroid of elements connected with this boundary. OPTION = SEGMENT_SET is for user defined meshes whereas OPTION = MSURF_SET is associated with the automatic volume mesher (See *MESH keywords).

That is, the MSURF_SET option is used when the dual CESE mesh has been created using *MESH cards. The SEGMENT_SET card is used when *DUALCESE_ELE2D or *DUALCESE_ELE3D cards are used to define the dual CESE mesh.

Card Sets:

A set of data cards for this keyword consists of 3 of the following cards:

- 1. Card 1 specifies the object to which the boundary condition is applied. Its format depends on the keyword option.
- 2. Card 2 reads in load curve IDs.
- 3. Card 3 reads in scale factors.

For each boundary condition to be specified include one set of cards. This input ends at the next keyword ("*") card.

Surface Part Set Card. Card 1 format used when the MSURF_SET keyword option is active.

Set Card. Card 1 format used when the SET keyword option is active.

Load Curve Card.

Scale Factor Card.

VARIABLE DESCRIPTION

MSURF_S Identifier of a set of mesh surface part IDs created with a *LSO_-ID_SET card, where each mesh surface part ID in the set is referenced in *MESH_SURFACE_ELEMENT cards.

SSID Segment set ID created with *DUALCESE_SEGMENTSET.

Remarks:

- 1. On each centroid or set of centroids, the variables (v_x , v_y , v_z , ρ , P , T) that are given values must be consistent and make the model well-posed (i.e., be such that the solution of the model exists, is unique and physical).
- 2. If any of the load curves are 0, the corresponding variable will take the constant value of the corresponding scale factor. For instance, if $LC_RHO = 0$, then the constant value of the density for this boundary condition will be SF_- RHO.
- 3. If a load ID is -1 for a given variable, then the boundary value for that variable is computed by the solver, and not specified by the user.

*DUALCESE_BOUNDARY_PRESCRIBED_VN_OPTION

Available options include:

MSURF_SET

SETMENT_SET

Purpose: For the dual CESE compressible flow solver, set boundary values for velocity, density, pressure and temperature. Boundary values are applied at the centroid of elements connected with this boundary. OPTION = SEGMENT_SET is for user defined meshes whereas OPTION = MSURF_SET is associated with the automatic volume mesher (See *MESH keywords).

That is, the MSURF_SET option is used when the dual CESE mesh has been created using *MESH cards. The SEGMENT_SET card is used when *DUALCESE_ELE2D or *DUALCESE_ELE3D cards is used to define the dual CESE mesh.

Card Sets:

A set of data cards for this keyword consists of 3 of the following cards:

- 1. Card 1 specifies the object to which the boundary condition is applied. Its format depends on the keyword option.
- 2. Card 2 reads in load curve IDs.
- 3. Card 3 reads in scale factors.

For each boundary condition to be specified include one set of cards. This input ends at the next keyword ("*") card.

Surface Part Set Card. Card 1 format used when the MSURF_SET keyword option is active.

*DUALCESE_BOUNDARY_PRESCRIBED_VN *DUALCESE

Set Card. Card 1 format used when the SEGMENT_SET keyword option is active.

Load Curve Card.

Scale Factor Card.

VARIABLE DESCRIPTION

MSURF_S Identifier of a set of mesh surface part IDs created with a *LSO_-ID_SET card, where each mesh surface part ID in the set is referenced in *MESH_SURFACE_ELEMENT cards.

SSID Segment set ID

Remarks:

- 1. On each centroid or set of centroids, the variables (V_N , ρ , P , T) that are given values must be consistent and make the model well-posed (i.e., be such that the solution of the model exists, is unique and physical).
- 2. If any of the load curves are 0, the corresponding variable will take the constant value of the corresponding scale factor. For instance, if $LC_RHO = 0$, then the constant value of the density for this boundary condition will be SF_- RHO.
- 3. If a load ID is -1 for a given variable, then the boundary value for that variable is computed by the solver, and not specified by the user.

*DUALCESE_BOUNDARY_REFLECTIVE_OPTION

Available options are:

MSURF_SET

SEGMENT_SET

Purpose: Define a reflective boundary condition (RBC) for the dual CESE compressible flow solver. This boundary condition can be applied on a symmetrical surface or a solid wall of the computational domain.

The MSURF_SET option is used when the dual CESE mesh has been created using *MESH cards. The SEGMENT_SET option is used when *DUALCESE_ELE2D or *DU-ALCESE ELE3D cards are used to define the dual CESE mesh.

Surface Part Set Card. Card 1 format used when the MSURF_SET keyword option is active. Provide as many cards as necessary. This input ends at the next keyword ("*") card.

Set Card. Card 1 format used when the SET keyword option is active. Provide as many cards as necessary. This input ends at the next keyword ("*") card.

VARIABLE DESCRIPTION

Remarks:

1. This boundary condition has the same effect as a solid-wall boundary condition for inviscid flows.

*DUALCESE_BOUNDARY_SOLID_WALL_OPTION1_OPTION2

For *OPTION1* the choices are:

MSURF_SET

SEGMENT_SET

For *OPTION2* the choices are:

<BLANK>

ROTAT

Purpose: Define a solid wall boundary condition (SBC) for the dual CESE compressible flow solver. This boundary condition can be applied at a solid boundary that is the physical boundary for the flow field. For inviscid flow, this will be a slip boundary condition; while for viscous flows, it is a no-slip boundary condition.

The MSURF_SET option is used when the dual CESE mesh has been created using *MESH cards. The SEGMENT_SET card is used when *DUALCESE_ELE2D or *DUAL-CESE_ELE3D cards are used to define the dual CESE mesh.

Card Sets. The following sequence of cards comprises a *single set*. LS-DYNA will continue reading *DUALCESE_BOUNDARY_SOLID_WALL card sets until the next keyword ("*") card is encountered.

Surface Part Set Card. Card 1 format used when the MSURF_SET keyword option is active.

Set Card. Card 1 format used when the SEGMENT_SET keyword option is active.

Rotating Axis Card. Additional card for the "Segment Card" case that is read when the ROTAT keyword option is used.

VARIABLE DESCRIPTION

MSURF_S Identifier of a set of mesh surface part IDs created with a *LSO_-ID_SET card, where each mesh surface part ID in the set is referenced in *MESH_SURFACE_ELEMENT cards.

- SSID Segment set ID created with *DUALCESE_SEGMENTSET.
- LCID Load curve ID to define this solid wall boundary movement

If OPTION2 = \leq BLANK $>$:

If OPTION2 = $ROTAT:$

Remarks:

- 1. In this solid-wall condition (SBC), the boundary movement can only be in the tangential direction of the wall and should not affect the fluid domain size and mesh during the calculation, otherwise an FSI or moving mesh solver should be used. Also, this moving SBC only affects viscous flows (no-slip BC).
- 2. If LCID = 0 and $Vx = Vy = Vz = 0.0$ (default), this will be a regular solid wall BC.
- 3. For rotating SBC, LCID > 0 must be used to define the rotating speed frequency (Hz). Also, in the 2D case, (Nx, Ny, Nz) does not need to be defined because it is not needed.

*DUALCESE_CONTROL_LIMITER

Purpose: Sets some stability parameters used in the dual CESE compressible flow solver on the current dual CESE model.

Remarks:

- 1. $\alpha \geq 0$; larger values give more stability, but less accuracy. Usually $\alpha = 2.0$ or 4.0 will be enough for normal shock problems.
- 2. $0 \le \beta \le 1$; larger values give more stability. For problems with shock waves, β = 1.0 is recommended.
- 3. $\varepsilon \geq 0$; larger values give more stability, but less accuracy.

*DUALCESE_CONTROL_MESH_MOV

Purpose: For the moving mesh dual CESE solver, this keyword is used to choose the type of algorithm to be used for calculating mesh movement.

VARIABLE DESCRIPTION

.

MMSH Mesh motion selector:.

EQ.9: the IDW scheme is used to move the mesh.

*DUALCESE_CONTROL_SOLVER

Purpose: Set general purpose control variables for the dual CESE compressible flow solver.

VARIABLE DESCRIPTION

ISNAN Flag to check for a NaN in the dual CESE solver solution arrays at the completion of each time step. This option can be useful for debugging purposes. There is a cost overhead when this option is active.

EQ.0: No checking,

EQ.1: Checking is active.

Remarks:

- 1. If the user wants to use the 2D (IGEOM = 2D) or 2D axisymmetric (IGE- $OM = AXI$) solver, the mesh should only be distributed in the x-y plane with the boundary conditions given only at the $x-y$ domain boundaries. Otherwise, a warning message will be given and the 3D solver will be triggered instead.
- 2. The 2D axisymmetric case will work only if the 2D mesh and corresponding boundary conditions are properly defined, with the x and y coordinates corresponding to the radial and axial directions respectively.
- 3. IDC is the same type of variable that is input on the *ICFD_CONTROL_FSI card. For an explanation, see Remark 1 for the *ICFD_CONTROL_FSI card.

*DUALCESE_CONTROL_TIMESTEP

Purpose: Sets the time-step control parameters for the CESE compressible flow solver.

*DUALCESE_**D3**PLOT

Purpose: Specify the flow variables to be added to the dual CESE d3plot output.

VARIABLE DESCRIPTION

Provide as many cards as necessary. This input ends at the next keyword ("*") card.

*DUALCESE_**D3PLOT_FLUID_SSID**

Purpose: Generate surface D3PLOT output for the dual CESE solver on a specified dual CESE mesh segment set. These surfaces may be on the outside of the dual CESE fluid mesh that is in contact with the structural volume element parts.

[Card 1.](#page-164-0) This card is required.

VARIABLE DESCRIPTION

SSID Segment set ID created with *DUALCESE_SEGMENTSET.

Dual CESE variables to output. Provide as many cards as necessary. This input ends at the next keyword ("*") card.

VARIABLE DESCRIPTION

FLOW_VAR Name of a flow variable to output to the d3plot file. The currently supported variables are: **DENSITY VELOCITY** MOMENTUM **VORTICITY** TOTAL_ENERGY INTERNAL_ENERGY PRESSURE TEMPERATURE ENTROPY ENTHALPY SCHLIEREN_NUMBER VOID_FRACTION

*DUALCESE *DUALCESE_ELE2D

*DUALCESE_ELE2D

Purpose: Define three and four node elements.

*DUALCESE_ELE3D

Purpose: Define three-dimensional fluid volume elements. These can be 4 node tetrahedrons, 5 node pyramids, 6 node wedges (prisms), and 8 node hexahedra.

Remarks:

1. Node Numbering. Four, five, six, and eight node elements are allowed as shown below. This ordering must be followed or code termination with occur during the initialization phase with a negative volume message. In the case of a pyramid element, the base of the pyramid must follow the ordering used for the hexahedron. See *ELEMENT_SOLID for a figure showing the positions of the nodes in 4, 6, and 8 node elements.

4-noded tetrahedron N1, N2, N3, N4, N4, N4, N4, N4

*DUALCESE *DUALCESE_ELE3D

*DUALCESE_ELEMENTSET

Purpose: Define a set of dual CESE mesh elements.

[Card 1.](#page-164-0) This card is required.

VARIABLE DESCRIPTION

ESID Set ID. All dual CESE element sets should have a unique set ID.

Element ID Cards. Set one value per node in the set. Include as many cards as needed. This input ends at the next keyword ("*") card.

VARIABLE DESCRIPTION

ELE*i* Element ID *i*

*DUALCESE_EOS_COOLPROP

Purpose: Define an equation of state (EOS) to be evaluated using the COOLPROP EOS library

Note that the COOLPROP library is not provided by ANSYS. The user needs to download a 64-bit version of the shared library from a public repository, such as: **https://sourceforge.net/projects/coolprop/files/CoolProp/6.3.0/shared_library/Linux/64 bit/**

As the *DUALCESE capability is not yet working in the Windows build of LS-DYNA, do not attempt to use a Windows DLL version of the COOLPROP shared library.

Next, in order to use the COOLPROP shared library with this keyword card, load this shared library into LS-DYNA using the *MODULE capability. The following *MOD-ULE card needs to appear before a *DUALCESE_MODEL card (not inside the file hierarchy of any file specified with a *DUALCESE_MODEL card).

***MODULE_LOAD**

UserA DUALCESE COOLPROP **< path to installed COOLPROP shared library >**

EOS Selection Card. Define a new COOLPROP EOS for use by a dual CESE solver.

COOLPROP Parameters by Fluid Component. Card 1 format repeated as many times as needed to input mole fractions for the NCOMP components of the fluid..

COOLPROP EOS Table Density and Temperature Ranges. Card 3 format used when the TABULAR option on Card 1 is active.

[Name of CoolProp fluid.](#page-164-0) This card is required.

VARIABLE DESCRIPTION

- EOSID Identifier for this EOS.
- NCOMP Number of components in the fluid composition

Remarks:

1.The number of values of density and temperature axes of the tables should not be too few to give good resolution of the EOS. Note that the cost of building the EOS from these tables rises with these numbers, as well as the computer memory required. Nevertheless, if these numbers are too small (< 20), then the accuracy may suffer, while larger numbers of density and temperature points improves the accuracy.

2.For many EOSes in the CoolProp library, there is a range of valid densities and temperatures. So the low and high limits for the table densities and temperatures should not lie outside these ranges. Please refer to the CoolProp documentation for that information..

*DUALCESE_EOS_IDEAL_GAS

Purpose: Define the coefficients **Cv** and **Cp** in the equation of state for an ideal gas in the dual CESE fluid solver.

VARIABLE DESCRIPTION

EOSID Equation of state identifier Cv Specific heat at constant volume Cp Specific heat at constant pressure

Remarks:

1. **Units.** As with other solvers in LS-DYNA, the user is responsible for unit consistency. For example, if a user wants to use dimensionless variables, Cv and Cp above also should be replaced by the corresponding dimensionless ones. If the dual CESE model has specified a system of units either directly in the *DUALCESE_MODEL card, or inherited a choice of units from the overall problem input, then these values need to be given in that unit system.

*DUALCESE_EOS_INFLATOR1

Purpose: To define an EOS using Cp and Cv thermodynamic expansions for an inflator gas mixture with a single temperature range.

VARIABLE DESCRIPTION

EOSID Equation of state identifier for the dual CESE solver.

Cp0, …, Cp4 Coefficients of temperature-dependent specific heat at constant pressure

 $C_p(T) = C_{p0} + C_{p1} T + C_{p2} T^2 + C_{p3} T^3 + C_{p4} T^4$

VARIABLE DESCRIPTION

Cv0, …, Cv4 Coefficients of temperature-dependent specific heat at constant volume

 $C_v(T) = C_{v0} + C_{v1} T + C_{v2} T^2 + C_{v3} T^3 + C_{v4} T^4$

Remark:

3.These coefficient expansions for the specific heats over the entire temperature range are generated by the 0-D inflator model solver. See *CHEMISTRY_CON-TROL_INFLATOR and *CHEMISTRY_INFLATOR_PROPERTIES for details related to running that solver.

*DUALCESE_EOS_INFLATOR2

Purpose: To define an EOS using Cp and Cv thermodynamic expansions for an inflator gas mixture with two temperature ranges, one below 1000 degrees Kelvin, and the other above 1000 degrees Kelvin.

Card for the expansion of Specific Heat at Constant Pressure. Valid for T < $1000\text{ }^{\circ}\text{K}$

Card for the expansion of Specific Heat at Constant Pressure. Valid for $T > 1000 \degree K$.

Card for the expansion of Specific Heat at Constant Volume. Valid for $T > 1000 \degree K$.

Remark:

4.These coefficient expansions for the specific heats over two temperature ranges are generated by the 0-D inflator model solver. See *CHEMISTRY_CONTROL_IN-FLATOR and *CHEMISTRY_INFLATOR_PROPERTIES for details related to running that solver.

*DUALCESE_EOS_REFPROP

Purpose: Define an equation of state (EOS) to be evaluated using the REFPROP EOS library

Note that the REFPROP library is not provided by ANSYS. The user needs to purchase REFPROP 9.1 from NIST. Then the user is required to build the REFPROP shared library from the fortran source files provided by NIST.

As the *DUALCESE capability is not yet working in the Windows build of LS-DYNA, do not attempt to use a Windows DLL version of the REFPROP shared library that comes with purchasing REFPROP 9.1.

Next, in order to use the REFPROP shared library with this keyword card, load this shared library into LS-DYNA using the *MODULE capability. The following *MOD-ULE card needs to appear before a *DUALCESE_MODEL card (not inside the file hierarchy of any file specified with a *DUALCESE_MODEL card).

*MODULE_LOAD UserA DUALCESE REFPROP <path to the installed REFPROP shared library>

In addition, in order for REFPROP to be able to find the appropriate EOS data when a *DUALCESE_EOS_REFPROP card is used in a problem, *DUAL-CESE_EOS_REFPROP_PATH must also be given somewhere inside a *DUALCESE_- MODEL file hierarchy to point to the place in the user's filesystem where REFPROP has been installed.

EOS Selection Card. Define a new REFPROP EOS for use by a dual CESE solver.

REFPROP Parameters by Fluid Component. Card 1 format repeated as many times as needed to input mole fractions for the NCOMP components of the fluid..

REFPROP EOS Table Density and Temperature Ranges. Card 3 format used when the TABULAR option on Card 1 is active.

[Name of REFPROP fluid.](#page-164-0) This card is required.

VARIABLE DESCRIPTION

- EOSID Identifier for this EOS.
- NCOMP Number of components in the fluid composition

Remarks:

1. The number of values of density and temperature axes of the tables should not be too few to give good resolution of the EOS. Note that the cost of building

the EOS from these tables rises with these numbers, as well as the computer memory required. Nevertheless, if these numbers are too small (< 20), then the accuracy may suffer, while larger numbers of density and temperature points improves the accuracy.

2. For many EOSes in the REFPROP library, there is a range of valid densities and temperatures. So the low and high limits for the table densities and temperatures should not lie outside these ranges. Please refer to the :REFPROP documentation for that information.

LS-DYNA R12 5-43 (DUALCESE)

*DUALCESE_EOS_REFPROP_PATH

Purpose: Provides the file path to the directory where the REFPROP EOS system is installed.

Note that in any problem where a *DUALCESE_EOS_REFPROP card is used, the user must also provide a *DUALCESE_EOS_REFPROP_PATH card somewhere inside a *DUALCESE_MODEL file hierarchy to point to the place in the user's filesystem where REFPROP has been installed so that the appropriate EOS data can be loaded.

REFPROP Directory Card.

VARIABLE DESCRIPTION

FILE Path giving the directory where the REFPROP data is installed.
*DUALCESE_**FSI_EXCLUDE**

Purpose: Provide a list of mechanics solver parts that are not involved in the dual CESE FSI calculation. This is intended to be used as an efficiency measure for parts that will not involve significant FSI interactions with the dual CESE compressible fluid solver.

Include as many cards as needed. This input ends at the next keyword ("*") card.

VARIABLE DESCRIPTION

PIDn IDs of mechanics parts that will be excluded from the FSI interaction calculation with the dual CESE solver.

*DUALCESE_INCLUDE_**MODEL**

Purpose: Provide the filename of a file containing more of the dual CESE model that overall forms one dual CESE model. Any number of these cards may be used in a single dual CESE model, where at top level, the overall model begins with a *DUAL-CESE_MODEL card.

VARIABLE DESCRIPTION

FILENAME Filename of the keyword file containing more of the dual CESE model. This card is only allowed inside a file that is given in one instance of a *DUALCESE_MODEL keyword card.

*DUALCESE_INITIAL

Purpose: Specify constant initial conditions (ICs) for flow variables at the centroid of each fluid element.

DESCRIPTION

U, V, W $x-$, $y-$, z-velocity components respectively RHO density $ρ$ P pressure Ρ T temperature Τ

Remarks:

- 1. **Required Input.** Usually, only two of ρ , $P \& T$ are needed to be specified (besides the velocity). If all three are given, only ρ and Ρ will be used.
- 2. **Applicable Elements.** These initial condition will be applied in those elements that have not been assigned a value by *DUALCESE_INITIAL_*OPTION* cards for individual elements or sets of elements.

*DUALCESE_INITIAL_OPTION

Available options include:

SET

ELEMENT

Purpose: Specify initial conditions for the flow variables at the centroid of each element in a set of elements or at the centroid of a single element.

Include as many cards as needed. This input ends at the next keyword ("*") card.

VARIABLE DESCRIPTION

EID/ESID Dual CESE element ID (**EID** from a *DUALCESE_ELE2D or *DU-ALCESE_ELE3D card), or dual CESE element set ID (**ESID** from a *DUALCESE_ELEMENTSET card).

- U, V, W $x-$, $y-$, z -velocity components respectively
	- RHO density
	- P pressure
	- T temperature

Remarks:

1. Usually, only two of ρ, Ρ and Τ are needed to be specified (besides the velocity). If all three are given, only ρ and Ρ will be used.

2. The priority of this card is higher than *DUALCESE_INITIAL, i.e., if an element is assigned an initial value by this card, *DUALCESE_INITIAL will no longer apply to that element.

*DUALCESE_MAT_GAS

Purpose: Define the fluid (gas) properties in a viscous flow for the dual CESE solver.

Include as many cards as needed. This input ends at the next keyword ("*") card.

VARIABLE DESCRIPTION

- MID Material identifier
- C1, C2 Two coefficients in the Sutherland's formula for viscosity, i.e.,

$$
\mu=\frac{C_1T^{\frac{3}{2}}}{T+C_2}
$$

where C_1 and C_2 are constants for a given gas. For example, for air at moderate temperatures,

 $C_1 = 1.458 \times 10^{-6}$ kg/msK^{1/2}, $C_2 = 110.4$ K

PRND The Prandtl Number (used to determine the coefficient of thermal conductivity). It is approximately constant for most gases. For air at standard conditions $PRND = 0.72$.

Remarks:

- 1. C1 and C2 are only used to calculate the viscosity in viscous flows, so for inviscid flows, this material card is not needed. The Prandtl number is used to extract the thermal conductivity, which is used when thermal coupling with the structure is activated.
- 2. As with other solvers in LS-DYNA, the user is responsible for unit consistency. For example, if dimensionless variables are used, C_1 and C_2 should be replaced by the corresponding dimensionless ones. If the dual CESE model has specified a system of units either directly in the *DUALCESE_MODEL card, or inherited

a choice of units from the overall problem input, then these values need to be given in that unit system. Also, note that the formulas here require the temperature be given in either Kelvin or Rankine units.

*DUALCESE_MAT_GAS_0

Purpose: Define the fluid (gas) properties in a viscous flow for the dual CESE solver.

Material Definition Cards. Include one card for each instance of this material type. This input ends at the next keyword ("*") card.

VARIABLE DESCRIPTION

Remarks:

- 1. The viscosity is only used viscous flows, so for inviscid flows, it is not necessary to define it. The thermal conductivity is only used to calculate the heat transfer between the structure and the thermal solver when coupling is activated.
- 2. As with other solvers in LS-DYNA, the user is responsible for unit consistency. For example, if dimensionless variables are used, MU should be replaced by the corresponding dimensionless one. If the dual CESE model has specified a system of units either directly in the *DUALCESE_MODEL card, or inherited a choice of units from the overall problem input, then these values need to be given in that unit system.

*DUALCESE_MAT_GAS_2

Purpose: Define the fluid (gas) properties in a viscous flow for the dual CESE solver.

Material Definition Cards. Include one card for each instance of this material type. This input ends at the next keyword ("*") card.

VARIABLE DESCRIPTION

MID Material identifier

MU0 / SMU Two coefficients appearing in the equation derived by combining Sutherland's formula with the Power law for dilute gases:

$$
\frac{\mu}{\mu_0} = \left(\frac{T}{T_0}\right)^{3/2} \frac{T_0 + S_\mu}{T + S_\mu}.
$$

where μ_0 is a reference value, and S_u is an effective temperature called the Sutherland constant, which is characteristic of the gas. For air at moderate temperatures,

$$
\mu_0 = 1.716 \times 10^{-5} \text{Ns/m}^2
$$
, $S_\mu = 111 \text{ K}$

K0/SK Two coefficients appearing in the equation derived by combining Sutherland's formula with the Power law for dilute gases:

$$
\frac{k}{k_0} = \left(\frac{T}{T_0}\right)^{3/2} \frac{T_0 + S_k}{T + S_k}
$$

where *k* is the thermal conductivity, k_0 is a reference value, and S_k is the Sutherland constant, which is characteristic of the gas. For air at moderate temperatures,

$$
k_0 = 0.0241 \, \text{W/m}, \qquad S_k = 194 \, \text{K}
$$

 T_0 Reference temperature. The default value (273.0) is for air, in degrees K.

Remarks:

- 1. Fields that Depend on Problem Physics. The viscosity is only used viscous flows, so for inviscid flows, it is not necessary to define it. The thermal conductivity is only used to calculate the heat transfer between the structure and the thermal solver when coupling is activated.
- 2. **Unit Consistency.** As with other solvers in LS-DYNA, the user is responsible for unit consistency. For example, if dimensionless variables are used, MU should be replaced by the corresponding dimensionless one. If the dual CESE model has specified a system of units either directly in the *DUALCESE_MOD-EL card, or inherited a choice of units from the overall problem input, then these values need to be given in that unit system.. Also, note that the formulas here require the temperature be given in either Kelvin or Rankine units.

*DUALCESE_**MODEL**

Purpose: Set the units used by a dual CESE compressible flow problem, along with the filename containing the dual CESE model. There can be any number of such models (each with a separate mesh), and each such model must be in a different file.

*DUALCESE_NODE2D

Purpose: Define a node and its coordinates in the global coordinate system. The nodal point ID must be unique relative to other nodes defined with *DUALCESE_NODE2D or *DUALCESE_NODE3D cards.

Node Cards. Include as many cards in the following format as desired. This input ends at the next keyword ("*") card.

VARIABLE DESCRIPTION

- NID Node number
- $X \sim x$ coordinate
- Y coordinate

*DUALCESE_NODE3D

Purpose: Define a node and its coordinates in the global coordinate system. The nodal point ID must be unique relative to other nodes defined with *DUALCESE_NODE3D or *DUALCESE_NODE2D cards.

Node Cards. Include as many cards in the following format as desired. This input ends at the next keyword ("*") card.

VARIABLE DESCRIPTION

NID Node number $X \sim x$ coordinate $Y \longrightarrow y$ coordinate Z *z* coordinate

*DUALCESE_NODESET

Purpose: Define a nodal set of dual CESE mesh nodes.

[Card 1.](#page-164-0) This card is required.

VARIABLE DESCRIPTION

NSID Set ID. All dual CESE node sets should have a unique set ID.

Node ID Cards. Set one value per node in the set. Include as many cards as needed. This input ends at the next keyword ("*") card.

VARIABLE DESCRIPTION

NSID ID of this node set.

NID*i* Node ID *i*

*DUALCESE_PART

Purpose: Define dual CESE solver parts, i.e., connect dual CESE material and EOS information. It also provides a means to restrict the type of solver used on a region of a dual CESE mesh. That is, an immersed boundary FSI solver, a moving mesh FSI solver, or a non-FSI Eulerian solver can be specified for just this part.

Part Cards. Include one card for each CESE part. This input ends at the next keyword ("*") card.

Card 1		$\overline{2}$	3	4	5	6	8
Variable	PID	MID	EOSID	FSITYPE	MOVMESH_ID		
Type				A			
Default	none	none	none	none	none		

Remarks:

1. Since material coefficients are only used in viscous flows, the MID can be left blank for inviscid flows.

*DUALCESE_SEGMENTSET

Purpose: Define a set of segments. For three-dimensional geometries, a segment can be triangular or quadrilateral. For two-dimensional geometries, a segment is a line defined by two nodes (with $N3 = N2$ and $N4 = N2$).

[Card 1.](#page-164-0) This card is required.

VARIABLE DESCRIPTION

SID Set ID. All segment sets should have a unique set ID.

Segment Cards. For each segment in the set include one card of this format unless the GENERAL option is used. Include as many cards as necessary. This input ends at the next keyword ("*") card.

VARIABLE DESCRIPTION

- N1 $\qquad \qquad$ Nodal point n_1
- N^2 Nodal point n_2
- N3 Nodal point n_3
- N4 Nodal point n_4 . To define a triangular segment, set $N4 = N3$.

FACE	Hexahedron	Pentahedron	Pyramid	Tetrahedron	
1	N1, N5, N8, N4	N1, N2, N5	N1, N4, N3, N2	N1, N2, N4	
$\overline{2}$	N ₂ , N ₃ , N ₇ , N ₆	N ₄ , N ₆ , N ₃	N1, N2, N5	N2, N3, N4	
3	N1, N2, N6, N5	N1, N4, N3, N2	N ₂ , N ₃ , N ₅	N1, N3, N2	
4	N ₄ , N ₈ , N ₇ , N ₃	N2, N3, N6, N5	N3, N4, N5	N1, N4, N3	
5	N1, N4, N3, N2	N1, N5, N6, N4	N ₄ , N ₁ , N ₅		
6	N ₅ , N ₆ , N ₇ , N ₈				

Table. Face definitions for volume dual CESE elements

*EM

The *EM keyword cards provide input for a new electromagnetism module for solving 3D eddy-current, inductive heating or resistive heating problems, coupled with mechanical and thermal solvers. Typical applications include magnetic metal forming and welding. A boundary element method in the air is coupled to finite elements in the conductor in order to avoid meshing the air.

*EM_2DAXI

*EM_BOUNDARY

*EM_BOUNDARY_PRESCRIBED

*EM_CIRCUIT

*EM_CIRCUIT_CONNECT

*EM_CIRCUIT_ROGO

*EM_CONTACT

*EM_CONTACT_RESISTANCE

*EM_CONTACT_SUBDOM

*EM_CONTROL

*EM_CONTROL_CONTACT

*EM_CONTROL_COUPLING

*EM_CONTROL_EROSION

*EM_CONTROL_SOLUTION

*EM_CONTROL_SWITCH

*EM_CONTROL_SWITCH_CONTACT

*EM_CONTROL_TIMESTEP

*EM_DATABASE_CIRCUIT

*EM_DATABASE_CIRCUIT0D

*EM_DATABASE_ELOUT

*EM_DATABASE_GLOBALENERGY

*EM_DATABASE_NODOUT

*EM_DATABASE_PARTDATA

*EM_DATABASE_POINTOUT

*EM_DATABASE_ROGO

*EM_DATABASE_TIMESTEP

*EM_EP_CELLMODEL_DEFINEFUNCTION

*EM_EP_CELLMODEL_FENTONKARMA

*EM_EP_CELLMODEL_FIZHUGHNAGUMO

*EM_EP_CELLMODEL_TENTUSSCHER

*EM_EOS_BURGESS

*EM_EOS_MEADON

*EM_EOS_PERMEABILITY

*EM_EOS_TABULATED1

*EM_EOS_TABULATED2

*EM_EXTERNAL_FIELD

*EM_ISOPOTENTIAL

*EM_ISOPOTENTIAL_CONNECT

*EM_ISOPOTENTIAL_ROGO

*EM_MAT_001

*EM_MAT_002

*EM_MAT_003

*EM_MAT_004

*EM_MAT_005

*EM_MAT_006

*EM_OUTPUT

*EM_POINT_SET

*EM_RANDLES_BATMAC

*EM_RANDLES_EXOTHERMIC_REACTION

*EM_RANDLES_MESHLESS

*EM_RANDLES_TSHELL

*EM_RANDLES_SHORT

*EM_RANDLES_SOLID

*EM_ROTATION_AXIS

*EM_SOLVER_BEM

*EM_SOLVER_BEMMAT

*EM_SOLVER_FEM

*EM_SOLVER_FEMBEM

*EM_2DAXI

Purpose: Sets up the electromagnetism solver as 2D axisymmetric instead of 3D, on a given part, in order to save computational time as well as memory.

The electromagnetism is solved in 2D on a given cross section of the part (defined by a segment set), with a symmetry axis defined by its direction (at this time, it can be the x , ν , or z axis). The EM forces and Joule heating are then computed over the full 3D part by rotations. The part needs to be compatible with the symmetry, i.e. each node in the part needs to be the child of a parent node on the segment set, by a rotation around the axis. Only the conductor parts (with a *EM_MAT_… of type 2 or 4) should be defined as 2D axisymmetric.

Remarks:

1. At this time, *either* all or none of the conductor parts should be 2D axisymmetric. In the future, a mix between 2D axisymmetric and 3D parts will be allowed.

*EM_BOUNDARY

Purpose: Define some boundary conditions for the electromagnetism problems.

Include as many cards as needed. This input ends at the next keyword ("*") card.

VARIABLE DESCRIPTION

SSID Segment Set Id

BTYPE EQ.9: The faces of this segment set are eliminated from the BEM calculations (used for example for the rear or side faces of a workpiece).

*EM_**BOUNDARY_PRESCRIBED**

Purpose: Prescribing a local boundary condition applied on nodes.

Optional Card.

Remarks:

1. This keyword is available for the Resistive heating solver (solver type 3) only for the moment.

*EM_CIRCUIT_{OPTION}

Available options include

SOURCE

Purpose: Define an electrical circuit.

For the SOURCE option, the current will be considered uniform in the circuit. In general, this is used to model stranded conductors carrying a source current (in which case Amperes become Ampere.turns). This can also be useful in order to save computational time in cases with a low frequency current and where the diffusion of the EM fields is a very fast process. This option is in contrast with the general case where the current density in a circuit is completed in accordance with the solver type defined in EMSOL of *EM_CONTROL. For example, if an eddy current solver is selected, the diffusion of the current in the circuit is taken into account.

VARIABLE DESCRIPTION

CIRCID Circuit ID

Table 6-1. Correspondence between circuit type and card entries. "M" indicates mandatory, "M*" mandatory with exceptions (see Remark 1), "O" indicates optional, and "-" indicates ignored.

Remarks:

- 1. When defining a circuit with an imposed current (type 1, 11 or 21) in cases of a closed loop geometry (torus), SIDVIN and SIDVOUT cannot be defined and thus, only SIDCURR is necessary.
- 2. When defining a circuit with an imposed tension (type 2, 12, 22), it is possible to also define SIDCURR. This can be useful in circuits where various flow

paths are possible for the current in order to force the entire current to go through SIDCURR.

3. Circuit types 21 and 22 are for cases where the periodic current/tension does not exactly follow a perfect sinusoidal. The user has to provide the shape of the current/tension over one period through a LCID as well as the frequency.

*EM_CIRCUIT_CONNECT

Purpose: This keyword connects several circuits together by imposing a linear constraint on the global currents of circuit pairs

$$
c_1 i_1 + c_2 i_2 = 0.
$$

This is especially useful for 2D axisymmetric models involving spiral or helical coils.

VARIABLE DESCRIPTION

- CONID Id of the Circuit Connect
- CONTYPE Type of connection between circuits. For the moment, it is only possible to combine circuits by imposing a linear constraint on the global current $(=1)$.
	- $C1/C2$ Values of the linear constraints if CONTYPE = 1.

*EM_CIRCUIT_ROGO

Purpose: Define Rogowsky coils to measure a global current vs time through a segment set or a node set.

Include as many cards as needed. This input ends at the next keyword ("*") card.

Remarks:

1. An ASCII file "em_rogo_xxx", with *xxx* representing the rogoId, is generated for each *EM_CIRCUIT_ROGO card giving the value of the current or the magnetic field vs time.

*EM_CONTACT

Purpose: Optional card used for defining and specifying options on electromagnetic contacts between two sets of parts. Generally used with the *EM_CONTACT_RESIS-TANCE card. Fields left empty on this card default to the value of the equivalent field for the [*EM_CONTROL_CONTACT](#page-220-0) keyword.

Contact Definition Cards. Include one card for each contact definition. This input ends at the next keyword ("*") card.

Remarks:

Contact is detected when *all of the following three condition are satisfied*:

1. Contact condition 1:

 $n_1 \cdot n_2 \leq -1 + \varepsilon_1$

2. Contact condition 2:

Figure 0-1. Contact detection conditions between two faces.

$$
-\varepsilon_2 \le \alpha_1 \le 1 + \varepsilon_2
$$

$$
-\varepsilon_2 \le \alpha_2 \le 1 + \varepsilon_2
$$

$$
-\varepsilon_2 \le \alpha_3 \le 1 + \varepsilon_2
$$

With n_1 and n_2 the normal vectors of faces f_1 and f_2 respectfully and P the projection of point a_2 on face f_1 with $(\alpha_1, \alpha_2, \alpha_3)$ its local coordinates (See Figure [0-1\)](#page-213-0).

- 3. Contact condition 3 depends on the contact type.
	- a) For contact type 0:

 $d \leq \varepsilon_3 S_1$

where *d* is the distance between *P* and a_2 and where S_1 the minimum side length:

 $S_1 = \min[d(a_1, b_1), d(b_1, c_1), d(c_1, a_1)]$

b) For contact type 1 :

 $d \leq D_0$

*EM_CONTACT_RESISTANCE

Purpose: Calculate the electric contact resistance of a previously defined EM contact in *EM_CONTACT.

- CONTID EM contact ID defined in *EM_CONTACT
- CTYPE Contact Resistance type :

EQ.1: Electric Contact resistance defined by user defined define function.

Figure 6-2. Electrode coming into contact with workpiece (RSW application).

VARIABLE DESCRIPTION

- JHRTYPE Indicates how the Joule heating calculated by the contact resistance shall be taken into account:
	- EQ.0: No addition: The Joule heating calculated by the contact resistance is not taken into account.
	- EQ.1: The Joule heating coming from the contact resistance is divided and distributed evenly among all elements neighboring the contact surface.

Remarks:

- 1. The parameters for the DEFINE_FUNCTION are :
	- a) time/emdt : current time and EM timestep.
	- b) arealoc/areatot : local area associated to each face in contact and total contact area.
	- c) ctdist : Contact distance between the two faces in contact.
*EM_CONTACT_SUBDOM

Purpose: Optional card used for defining a specific region where EM contact will be active. This allows saving some calculation time by limiting the contact search area. Must be used in conjunction with *EM_CONTROL_CONTACT.

*EM_CONTROL

Purpose: Enable the EM solver and set its options.

VARIABLE DESCRIPTION

NCYLBEM Number of electromagnetism cycles between the recalculation of BEM matrices. If a negative value is entered, then the absolute value will refer to a load curve giving NCYCLBEM function of time.

*EM_CONTROL_CONTACT

Purpose: This keyword activates the electromagnetism contact algorithms, which detects contact between conductors. Electromagnetic fields flow from one conductor to another when detected as in contact.

- 1. In versions prior to R12, CTYPE = 0 was the default EM contact for the resistive heating solver while CTYPE = -1 was the default EM contact for the Eddy current solver. $CTYPE = 1$ and $CYPE = 2$ are the recommended contacts for best accuracy.
- 2. When the Eddy current solver is active, when contact occurs between BEM surfaces, the solver will automatically remove the faces that are on the contact surface and internally stitch the two BEM surfaces together in order to achieve a continuous closed BEM mesh.

*EM_CONTROL_COUPLING

Purpose: Allows the user to control couplings between various solvers with the EM solver.

VARIABLE DESCRIPTION

SMCPLFL Interaction between the solid mechanics solver and the ICFD solver when EM quantities are solved on fluid elements.

> EQ.0: Default FSI. The fluid pressure will be passed to the solid mechanics solver.

 EQ.1: The fluid pressure is replaced by the electrostatic pressure.

 EQ.2: Both the fluid pressure and the electrostatic pressure are passed on to the solid mechanics solver.

*EM_CONTROL_EROSION

Purpose: Allows the EM solver to take eroded elements into account

VARIABLE DESCRIPTION

ECTRL Erosion search :

- EQ.0: Off. This means that the EM solver will ignore eroded elements and still consider them part of the EM problem.
- EQ.1: On. The EM solver will look for potential elements that are eroded and remove them from the EM solve by updating its matrix system.

*EM_CONTROL_SOLUTION

Purpose: Allows the user to specify different conditions under which the FEM and BEM matrices are reassembled.

VARIABLE DESCRIPTION

- NCYLFEM Number of electromagnetism cycles between the recalculation of FEM matrices. If a negative value is entered, then the absolute value will refer to a load curve giving NCYCLFEM function of time.
- NCYLBEM Number of electromagnetism cycles between the recalculation of BEM matrices. If a negative value is entered, then the absolute value will refer to a load curve giving NCYCLBEM function of time.
- AUTOFEM In addition to NCYLFEM, this triggers an automatic recomputation of the FEM matrices based on an error calculation of the conductors' relative deformation and electrical conductivity changes. See TOL1FEM and TOL2FEM.
	- EQ.0: Autorecomputation off.
	- EQ.1: Autorecomputation on.
- AUTOBEM In addition to NCYLBEM, this triggers an automatic recomputation of the BEM matrices based on an error calculation of the conductors' relative displacements. See TOL1BEM and TOL2BEM.
	- EQ.0: Autorecomputation off.
	- EQ.1: Autorecomputation on.

VARIABLE DESCRIPTION TOL1FEM If a conducting element sees a deformation or a conductivity change that reaches an error higher than TOL1FEM, then the FEM matrices will be reassembled. If a negative value is entered, then the absolute value will refer to a load curve giving TOL1FEM function of time. TOL2FEM If TOL2FEM*Number-of-conducting-elements see a deformation or a conductivity change that reaches an error higher than TOL2FEM, then the FEM matrices will be recomputed. If a negative value is entered, then the absolute value will refer to a load curve giving TOL2FEM function of time. TOL1BEM If a conducting element sees a displacement that reaches an error higher than TOL1BEM, then the BEM matrices will be reassembled. If a negative value is entered, then the absolute value will refer to a load curve giving TOL1BEM function of time. TOL2BEM If TOL2BEM*Number-of-conducting-elements see a displacement that reaches an error higher than TOL2BEM, then the BEM matrices will be recomputed. If a negative value is entered, then the absolute value will refer to a load curve giving TOL2BEM function of time.

*EM_CONTROL_SWITCH

Purpose: It is possible to active a control "switch" that will shut down the solver based on a load curve information. LS-DYNA incorporates complex types of curves (See *DE-FINE_CURVE_FUNCTION) that allow the setting up of complex On/Off switches, for instance, by using a nodal temperature value.

*EM_CONTROL_SWITCH_CONTACT

Purpose: It is possible to active a control "switch" that will shut down the electromagnetic contact detection. This can be useful in order to save some calculation time in cases where the user knows when contact between conductors will occur or stop occurring.

VARIABLE DESCRIPTION

LCID Load Curve ID.

Negative values switch the contact detection off, positive values switch it back on.

- NCYLFEM Determines the number of cycles before FEM matrix recomputation. If defined this will overwrite the previous NCY-CLFEM as long as the contact detection is turned on.
- NCYLBEM Determines the number of cycles before BEM matrix recomputation. If defined this will overwrite the previous NCY-CLBEM as long as the contact detection is turned on.

*EM_CONTROL_TIMESTEP

Purpose: Controls the EM time step and its evolution.

EQ.0: Default. The EM time step will go below the solid

VARIABLE DESCRIPTION

mechanics timestep, and several EM solves will occur between two solid mechanics time steps to ensure time consistency.

EQ.1: The solid mechanics time step will adapt and decrease to the EM time step value so that only one EM solve occurs between two solid mechanics solves.

Remarks:

1. Eddy Current Solver Automatic Time Step. For an eddy current solver, the automatic time step is based on the diffusion equation for the magnetic field:

$$
\sigma \frac{\partial \vec{A}}{\partial t} + \vec{\nabla} \times \frac{1}{\mu} \vec{\nabla} \times \vec{A} + \sigma \vec{\nabla} \varphi = \vec{j}_S.
$$

It is computed as the minimal elemental diffusion time step over the elements. For a given element, the elemental diffusion time step is given as $dt_e = l_e^2/(2D)$, where:

- *D* is the diffusion coefficient $D = 1/(\mu_0 \sigma_e)$,
- σ_e is the element electrical conductivity,
- μ_0 is the permeability of free space,
- • l_e is the minimal edge length of the element (minimal size of the element).
- 2. Automatic Time Step with RLC Circuit. When an automatic time step is defined and an RLC circuit is present, the EM solver will perform an additional check and calculate an approximation of the first current period based on a 0-D circuit solve. It will then limit the timestep by a factor $T_{\text{period}}/(4 \times \text{RLCSF})$. The default value of RLCSF ensures that 25 EM timesteps will be calculated for the first quarter period.
- 3. **MECATS.** In general, we recommend avoiding scenarios where the EM time step becomes smaller than the solid mechanics time step which are often the result of ill-defined input decks and parameters. This can, however, happen in cases where conducting elements have high deformations and an automatic EM time step is selected in which case you can choose between the two MECATS options.

*EM_DATABASE_CIRCUIT

Purpose: This keyword enables the output of EM data for every circuit defined.

Output options card

- 1. The file name for this database is em_circuit_XXX.dat with XXX the circuit ID.
- 2. ResistanceD is calculated in the following way:
	- a) A scalar potential difference of 1 is imposed at the circuit's boundaries SIDVIN and SIDVOUT.
	- b) The system to be solved at SIDCURR is then $\nabla^2 \varphi = 0$ with $\varphi_{\text{SIDVIN}} = 1$ and $\varphi_{\text{SIDVOUT}} = 0$. No diffusive effects are taken into account meaning that the current density can be written as $\mathbf{j} = \nabla \varphi$ and the total current as $I = \mathbf{j} \cdot \mathbf{k}$ $\mathbf{n}dA$.
	- c) The resistance can then be estimated using $R_D = U/I$. The calculation of this R_D resistance is solely based on the circuit's geometry and conductivity. It is therefore equivalent to the resistance as commonly defined in the circuit equations:

$$
R_D=L/\sigma S
$$

where L is the length of the circuit and S its surface area.

- 3. ResistanceJ is calculated by using the data provided during the EM solve : $R_I = J/I^2$ where J and I are, respectively, the joule heating and the current. Compared with ResistanceD, ResistanceJ is not so much a resistance calculation since it accounts for the resistive effects (when using the Eddy current solver). Rather, it corresponds to the resistance that the circuit would need in order to get the same Joule heating in the context of a circuit equation. If all EM fields are diffused or the RH solver is being used, ResistanceJ should be close to ResistanceD.
- 4. Only the mutual inductances between the first three circuits defined are output.

*EM_DATABASE_CIRCUIT0D

Purpose: This keyword enables the output of EM data for every circuit defined.

Output options card

- 1. The file name for this database is em_circuit0D_XXX.dat with XXX the circuit ID.
- 2. At the start of the run, based on the initial values of the meshes resistances and inductances, the solver will calculate the results for a so-called "0D" solution which does not take into account the current's diffusion, the part's displacements or the EM material property changes. It is therefore a crude approximation. This can be useful in some cases especially in R,L,C circuits if the users wishes to have an first idea of how the source current will behave.
- 3. Since the calculation of this 0D circuit can take time depending on the problems size, it should only be used in cases where the output results are useful to the comprehension of the analysis.
- 4. This card has no influence on the results of the EM run itself.

*EM_DATABASE_**ELOUT**

Purpose: This keyword enables the output of EM data on elements.

Output Options Card.

Include as many cards as needed. This input ends at the next keyword ("*") card.

Remarks:

1. The file name for this database is em_elout.dat.

*EM_**DATABASE_FIELDLINE**

Purpose: The EM solver uses a BEM method to calculate the EM fields between conductors. With this method, the magnetic field in the air or vacuum between conductors is therefore not explicitly computed. However, in some cases, it may be interesting to visualize some magnetic field lines for a better analysis. This keyword allows the output of field line data. It has no influence on the results of the EM solve.

Output Options Card.

Remaining cards are optional.†

*EM_DATABASE_FIELDLINE *EM

- 1. File Names. The file name for this database is em_fieldLine_XX_YYY.dat where XX is the field line ID and YYY is the point set ID defined in *EM_- POINT_SET.
- 2. **Integrators.** The Runge Kutta 4 integrator is an explicit iterative method for solving ODEs. It is a fourth order method with a constant step size. The Dormand Prince 8(5,3) integrator is an explicit iterative method for solving IDEs. Particularly, this integrator is an embedded Runge Kutta integrator of order 8 with an adaptive step size. This integrator allows a step size control which is done though an error estimate at each step. The Dormand Prince 8(5,3) is a Dormand Prince $8(6)$ for which the $6th$ order error estimator has been replaced by a $5th$ order estimator with $3rd$ order correction in order to make the integrator more robust.

*EM_DATABASE_GLOBALENERGY

Purpose: This keyword enables the output of global EM.

Output Options Card.

- 1. The file name for this database is em_globEnergy.dat.
- 2. Outputs the global EM energies of the mesh, the air and the source circuit. Also outputs the global kinetic energy and the global plastic work energy.

*EM_DATABASE_**NODOUT**

Purpose: This keyword enables the output of EM data on nodes.

Output Options Card.

Include as many cards as needed. This input ends at the next keyword ("*") card.

Remarks:

1. The file name for this database is em_nodout.dat.

*EM_DATABASE_PARTDATA

Purpose: This keyword enables the output of EM data for every part defined. .

Output Options Card.

- 1. The file name for this database is em_partData_XXX.dat with XXX the part ID.
- 2. Outputs the part EM energies of the part as well as the Lorentz force. Also outputs the part kinetic energy and the part plastic work energy.

*EM_DATABASE_**POINTOUT**

Purpose: This keyword enables the output of EM data on points sets.

Output Options Card.

Include as many cards as needed. This input ends at the next keyword ("*") card.

Remarks:

1. The file name for this database is em_pointout.dat.

*EM_DATABASE_ROGO

Purpose: This keyword enables the output of EM data for every circuit defined. .

Output Options Card.

Remarks:

1. The file name for this database is em_rogoCoil_XXX.dat where XXX is the rogo Coil ID.

*EM_DATABASE_**TIMESTEP**

Purpose: This keyword enables the output of EM data regarding the EM timestep.

Output options card.

VARIABLE DESCRIPTION

OUTLV Determines if the output file should be dumped.

EQ.0: No output file is generated.

EQ.1: The output file is generated.

- 1. The file name for this database is em_timestep.dat.
- 2. Outputs the run's EM tim estep versus the time step calculated using the EM CFL condition as criteria (autotimestep). This can be useful in cases with big deformations and/or material property changes and a fixed time step is being used in case that time step becomes to big compared to the stability time step.

*EM_**EP_CELLMODEL_DEFINEFUNCTION**

Purpose: Define a user defined ionic cell model for Electro-Physiology.

VARIABLE DESCRIPTION

MATID Material ID defined in the *MAT section

FSWITCH Switch for the ODE definition (see Remark 1):

EQ.0: functions

EQ.1: derivatives

VARIABLE DESCRIPTION

Remarks:

1. This allows having a user defined cell model defined through define functions (See *DEFINE_FUNCTION). The model is composed of the transmembrane potential, V, along with *n* state variables $u_1, u_2, \ldots u_n$. Their temporal evolution is given depending upon FSWITCH.

a) If
$$
FSWITCH = 0
$$
:

$$
V(t) = g(t, dt, V(t-1), u_1(t-1), u_2(t-1), ..., u_n(t-1))
$$

\n
$$
u_1(t) = f_1(t, dt, V(t-1), u_1(t-1), u_2(t-1), ..., u_n(t-1))
$$

\n
$$
u_2(t) = f_2(t, dt, V(t-1), u_1(t-1), u_2(t-1), ..., u_n(t-1))
$$

\n
$$
\vdots
$$

\n
$$
u_n(t) = f_n(t, dt, V(t-1), u_1(t-1), u_2(t-1), ..., u_n(t-1))
$$

b) If $FSWITCH = 1$:

$$
\frac{\partial V(t)}{\partial t} = g(t, dt, V(t-1), u_1(t-1), u_2(t-1), \dots, u_n(t-1))
$$

\n
$$
\frac{\partial u_1(t)}{\partial t} = f_1(t, dt, V(t-1), u_1(t-1), u_2(t-1), \dots, u_n(t-1))
$$

\n
$$
\frac{\partial u_2(t)}{\partial t} = f_2(t, dt, V(t-1), u_1(t-1), u_2(t-1), \dots, u_n(t-1))
$$

\n
$$
\vdots
$$

\n
$$
\frac{\partial u_n(t)}{\partial t} = f_3(t, dt, V(t-1), u_1(t-1), u_2(t-1), \dots, u_n(t-1))
$$

2. Benchmarks. The electrophysiology benchmarks presented in:

[1] "Verification of computational models of cardiac electro-physiology", Pathmanathan P, Gray RA., Int J Numer Method Biomed Eng. 2014 May;30(5):525-44

can be done with this model.

*EM_**EP_CELLMODEL_FENTONKARMA**

Purpose: Define an Fenton-Karma ionic cell model for Electro-Physiology.

Remarks:

1. The Fenton-Karma model is a simplified ionic model with three membrane currents that approximates well the restitution properties and spiral wave behavior of more complex ionic models of cardiac action potential (Beeler-Reuter and others). It was introduced in [1]

$$
I_{ion} = -C_m \frac{\partial V}{\partial t} = -J_{fi} \tag{1}
$$

Where *V* is the transmembrane potential, C_m the specific capacitance of the cell membrane.

$$
\frac{du}{dt} = -J_{fi} - -J_{fo} - J_{si}
$$
 (2)

$$
\frac{dv}{dt} = \frac{\Theta(u_c - u)(1 - v)}{\tau_{vm}} - \frac{\Theta(u - u_c)v}{\tau_{vp}}
$$
(3)

$$
\frac{dw}{dt} = \frac{\Theta(u_c - u)(1 - w)}{\tau_{wm}} - \frac{\Theta(u - u_c)w}{\tau_{wp}}\tag{4}
$$

$$
J_{fi} = -\frac{\Theta(u_c - u)(1 - u)(u - u_c)}{\tau_d} \tag{5}
$$

$$
J_{so} = \frac{u \Theta(u_c - u)}{\tau_o} + \frac{u \Theta(u - u_c)}{\tau_r}
$$
\n
$$
\tag{6}
$$

$$
J_{si} = -\frac{w(1 + \tanh[k(u - u_c^{si}]))}{2\tau_{si}}
$$
 (7)

Where Θ is the Heaviside step function.

2. References:

[1] "Vortex dynamics in three-dimensional continuous myocardium with fiber rotation: Filament instability and fibrillations", F. Fenton and A.Karma, Chaos, Solitons and Fractals, Vol 8 No 1, pp 20-47, 1998

[2] https://www.ibiblio.org/e-notes/html5/fk.html

*EM_EP_CELLMODEL_FITZHUGHNAGUMO

Purpose: Define an Fitzhugh-Nagumo ionic cell model for Electro-Physiology.

Remarks:

1. In the Fitzhugh-Nagumo model, the excitation is defined by a cubic polynomial along with one recovery variable, r . The transmembrane current reads :

$$
I_{ion} = -C_m \frac{\partial V}{\partial t} = -cV (V - \alpha)(V - 1) - rV
$$
\n(1)

Where *V* is the transmembrane potential, C_m the specific capacitance of the cell membrane and c and α are excitation constants.

The recovery variable r evolves according to :

$$
\frac{dr}{dt} = (\gamma + \frac{r\mu_1}{\mu_2 + V})(-r - cV(V - \beta - 1))\tag{2}
$$

Where β, γ , μ_1 and μ_2 are excitation constants.

2. References:

[1] "A simple Two-variable Model of Cardiac Excitation", R.R. Aliev and A.V. Panfilov, Chaos, Solitons and Fractals, Vol 7 No 3, pp 293-301, 1996

[2] "Mathematically modelling the electrical activity of the heart", A.J. Pullan et Al., World Scientific Publishing Co. Pte. Ltd., Singapore, 2005, pp 132-133

[3] "The living heart Project: A robust and integrative simulator for human heart function", B. Baillargeon et Al., European Journal of Mechanics A/solids 48 (2014), pp 38-47
*EM_**EP_CELLMODEL_TENTUSSCHER**

Purpose: Define a ten Tusscher ionic cell model for Electro-Physiology.

Card Summary:

[Card 11.](#page-258-0) This card is required.

Data Card Definitions:

VARIABLE DESCRIPTION

MID Material ID defined in *MAT section

VARIABLE DESCRIPTION

R Gas constant $(J \times K^{-1} \times Mol^{-1})$

T Temperature (K)

*EM_EP_CELLMODEL_TENTUSSCHER *EM

VARIABLE DESCRIPTION

- KO Extracellular K⁺ concentration (mM)
- NAO Extracellular Na⁺ concentration (mM)
- CAO Extracellular Ca^{2+} concentration (mM)

GK1, GKR, GKS, GNA, GBNA, GCAL, GB-CA, GTO, GPCA, GPK

Maximal I_{K1} , I_{Kr} , I_{Ks} , I_{Na} , I_{bNa} , I_{Cal} , I_{bCa} , I_{to} , I_{pCa} , and I_{pK} conductance, respectively (units: $nS \times pF^{-1}$)

VARIABLE DESCRIPTION

PNAK P_{Nak} , parameter for calculating the Na+/K+ pump current (units: $pA \times pF^{-1}$). See Reference [\[1\]](#page-260-0).

DESCRIPTION

XR1 Initial value of x_{r1} , used to compute the rapid time dependent K⁺ current

Remarks:

This is a model of the action potential of human ventricular cells that, while including a high level of electrophysiological detail, is computationally cost-effective enough to be applied in large-scale spatial simulations for the study of reentrant arrhythmias. Please see the references for details. This model is based on [\[2\]](#page-260-1).

References:

[1] "A model for human ventricular tissue", K.H.W.J. ten Tusscher et Al., Am J Physiol Heart Circ Physiol 286: H1573-H1589, 2004

[2] "Alternans and spiral breakup in human ventricular tissue model", K.H.W.J. ten Tusscher and A.V. Panfilov, Am J Physiol Heart Circ Physiol 291: H1088-H1100, 2006

*EM_EOS_BURGESS

Purpose: Define the parameters for a Burgess model giving the electrical conductivity as

as a function of the temperature and the density, see:

T.J. Burgess, "Electrical resistivity model of metals", 4th International Conference on Megagauss Magnetic-Field Generation and Related Topics, Santa Fe, NM, USA, 1986

In the following, UUS stands for User Units System and BUS for Burgess Units

*EM_EOS_BURGESS *EM

Remarks:

1. The Burgess model gives the electrical resistivity vs temperature and density for the solid phase, liquid phase and vapor phase. At this time, only the solid and liquid phases are implemented. To check which elements are in the solid and in the liquid phase, a melting temperature is first computed by:

$$
\theta_m = \theta_{m,0} \left(\frac{V}{V_0}\right)^{-\frac{1}{3}} e^{(2\gamma_0 - 1)(1 - \frac{V}{V_0})}
$$

a) If $T < \theta_m$: solid phase model applies.

The solid phase electrical resistivity corresponds to the Meadon model:

$$
\eta_S = (C_1 + C_2 \theta^{C_3}) f_c \left(\frac{V}{V_0}\right), \tag{1}
$$

where $θ$ is the temperature, V is the specific volume, and V_0 is the reference specific volume (zero pressure, solid phase). In [\(1\),](#page-263-1) the volume dependence is given by:

$$
f_c\left(\frac{V}{V_0}\right) = \begin{cases} \left(\frac{V}{V_0}\right)^{2\gamma - 1} & \text{(most materials)}\\ \left(\frac{V}{V_0}\right)^{2\gamma + 1} & \text{(tungsten)}\\ \left(\frac{V}{V_0}\right)^{2\gamma} & \text{EXPON.EQ. +1} \end{cases}
$$
(2)
EXPON.EQ. 0 (stainless steel)

with

$$
\gamma = \gamma_0 - \left(\gamma_0 - \frac{1}{2}\right) \left(1 - \frac{V}{V_0}\right) \tag{3}
$$

b) If $T > \theta_m$ iquid phase model:

$$
\eta_L = (\eta_L)_{\theta_m} \left(\frac{\theta}{\theta_m}\right)^{C_4} \tag{4}
$$

with

$$
(\eta_L)_{\theta_m} = \Delta \eta(\eta_S)_{\theta_m}
$$

where

$$
\Delta \eta = \begin{cases}\nk e^{0.69 L_F / \theta_m} & k > 0 \\
1 + 0.0772(2 - \theta_m) & k = -1 \\
1 + 0.106(0.846 - \theta_m) & k = -2 \quad \text{(stainless steel SS-304)}\n\end{cases}
$$
\n(5)

The following table reports some sets of parameters given by Burgess in his paper:

*EM_EOS_MEADON

Purpose: Define the parameters for a Meadon model, giving the electrical conductivity as a function of the temperature and the density; see:

T.J. Burgess, "Electrical resistivity model of metals", 4th International Conference on Megagauss Magnetic-Field Generation and Related Topics, Santa Fe, NM, USA, 1986

In the following, UUS stands for User Units System and BUS for Burgess Units.

*EM_EOS_MEADON *EM

Remarks:

1. The Meadon model is a simplified Burgess model with the solid phase equations only.

The electrical resistivity is given by:

$$
\eta_S = \left(C_1 + C_2 \theta^{C_3}\right) f_c \left(\frac{V}{V_0}\right) \tag{6}
$$

where $θ$ is the temperature, V is the specific volume, and V_0 is the reference specific volume (zero pressure, solid phase).

In (6) , the volume dependence is given by:

$$
f_c\left(\frac{V}{V_0}\right) = \begin{cases} \left(\frac{V}{V_0}\right)^{2\gamma - 1} & \text{(most materials)}\\ \left(\frac{V}{V_0}\right)^{2\gamma + 1} & \text{(tungsten)}\\ \left(\frac{V}{V_0}\right)^{2\gamma} & \text{EXPON.EQ.} + 1 \end{cases}
$$
 (tungsten) (7)
EXPON.EQ.0 (stainless steel)
1 VO.EQ.0 (default value for V_0 is zero)

 (In this last case, only EOSID, C1, C2, C3, TEMUNIT, TIMUNIT and LGTUNIT need to be defined)

with,

$$
\gamma = \gamma_0 - \left(\gamma_0 - \frac{1}{2}\right) \left(1 - \frac{V}{V_0}\right) \tag{8}
$$

The following table reports some sets of parameters given by Burgess in his paper:

*EM_EOS_PERMEABILITY

Purpose: Define the parameters for the behavior of a material's permeability

*EM_EOS_TABULATED1

Purpose: Define the electrical conductivity as a function of temperature by using a load curve.

VARIABLE DESCRIPTION

Remarks:

1. The load curve describes the electrical conductivity (ordinate) vs the temperature (abscissa). The user needs to make sure the temperature and the electrical conductivity given by the load curve are in the correct units. Also, it is advised to give some bounds to the load curve (conductivities at very low and very high temperatures) to avoid bad extrapolations of the conductivity if the temperature gets out of the load curve bounds.

*EM_EOS_TABULATED2

Purpose: Define the electrical conductivity as a function of time by using a load curve.

Remarks:

- 1. The load curve describes the electrical conductivity (ordinate) vs the time (abscissa). The user needs to make sure the time and the electrical conductivity given by the load curve are in the correct units. Also, it is advised to give some bounds to the load curve (conductivities at $t = 0$ at after a long time) to avoid bad extrapolations of the conductivity if the run time gets out of the load curve bounds.
- 2. LCID can also refer to a DEFINE FUNCTION. If a DEFINE FUNCTION is used, the following parameters are allowed: $f(vx, vy, vz, temp, pres, vol, mass, Ex, Ey, Ez, Bx, By, Bz, Fx, Fy, Fz, JH rate, time).$ Fx, Fy, Fz refers to the Lorentz force vector.

*EM_EXTERNAL_FIELD

Purpose: Define the components of a time dependent exterior field uniform in space applied on the conducting parts.

Remarks:

1. **Electrostatic Problems.** FTYPE $= 3$ is mostly used in electrostatic problem configurations. The material's conductivity then represents the permittivity.

*EM_**ISOPOTENTIAL**

Purpose: Defining an isopotential, i.e. constrain nodes so that they have the same scalar potential value. This card is to be used with the EM solver of type 3.

*EM_**ISOPOTENTIAL_CONNECT**

Purpose: Define a connection between two isopotentials or between an isopotential and the ground.

R,L,C circuit parameters. Only to be defined if CONTYPE = 6.

DESCRIPTION

CONID Connection ID

CONTYPE Connection type :

- EQ.1: Short Circuit.
- EQ.2: Resistance.
- EQ.3: Voltage Source.
- EQ.4: Current Source.
- EQ.5: Meshless Randles circuit (used to represent a cell by one lumped Randles circuit)
- EQ.6: R, L, C circuit
- ISOID1 ID of the first isopotential to be connected

*EM_**ISOPOTENTIAL_ROGO**

Purpose: measures the total current flowing through a given section of the conductor and outputs it in an ASCII file called em_rogoCoil.dat

VARIABLE DESCRIPTION

- ISOID ID of the Rogo coil.
- SETTYPE Set type:
	- EQ.1: Segment Set.

SETID Set ID

*EM_MAT_001

Purpose: Define the electromagnetic material type and properties for a material whose permeability equals the free space permeability.

- DEATHT Death time for the material. After DEATHT, the material will no longer be considered a conductor and removed from the EM solve. If a negative value is entered, a *DEFINE_FUNCTION will be expected. The following parameters are allowed: *(vx, vy, vz, temp, vol, mass, Ex, Ey, Ez, Bx, By, Bz, Fx, Fy, Fz, JHrate, time)* . *Fx, Fy, Fz* refers to the Lorentz force vector. A negative value returned by the *DEFINE_FUNCTION corresponds to a 'dead' or inactive element. Once an element has been removed from the EM solve, it cannot return.
- RDLTYPE Used for the application: composite Tshell battery, with $*EM$ -RANDLES_TSHELL . Defines the function of the layer associated to MID:
	- EQ.1: Current Collector Positive
	- EQ.2: Positive Electrode
	- EQ.3: Separator
	- EQ.4: Negative Electrode
	- EQ.5: Current Collector Negative

Remarks:

1. Only the resistive heating solver is currently available when coupling the ICFD solver with the EM solver (see *EM_CONTROL).

*EM_MAT_002

Purpose: Define an electromagnetic material type and properties whose permeability is different than the free space permeability.

DEATHT Death time for the material. After DEATHT, the material will no longer be considered a conductor and removed from the EM solve. If a negative value is entered, a *DEFINE_FUNCTION will be expected. The following parameters are allowed: *(vx, vy, vz, temp, vol, mass, Ex, Ey, Ez, Bx, By, Bz, Fx, Fy, Fz, JHrate, time)* . *Fx, Fy, Fz* refers to the Lorentz force vector. A negative value returned by the *DEFINE_FUNCTION corresponds to a 'dead' or inactive element. Once an element has been removed from the EM solve, it cannot return.

*EM_**MAT_003**

Purpose: Define an electromagnetic material type whose electromagnetic conductivity is defined by a (3*3) tensor matrix. Applications include composite materials.

Orthotropic Card 1.

Orthotropic Card 2.

Orthotropic Card 3.

Orthotropic Card 4.

VARIABLE DESCRIPTION

MID Material ID: refers to MID in the *PART card.

Define AOPT for both options:

defined by the cross product of the vector v with the element normal. The plane of a solid element is the midsurface between the inner surface and outer surface defined by the first four nodes and the last four nodes of the connectivity of the element, respectively.

- EQ.4.0: locally orthotropic in cylindrical coordinate system with the material axes determined by a vector v, and an originating point, P, which define the centerline axis. This option is for solid elements only.
- EQ.5.0: globally defined reference frame with $(a,b,c)=(X0,Y0,Z0).$
- XP, YP, ZP Define coordinates of point **p** for AOPT = 1 and 4.
- A1, A2, A3 Define components of vector **a** for AOPT = 2.
- MACF Material axes change flag for solid elements: EQ.1: No change, default,
- V1, V2, V3 Define components of vector **v** for AOPT = 3 and 4.
- D1, D2, D3 Define components of vector **d** for AOPT = 2.

Remarks:

This card works in a similar way to *MAT_002.

The procedure for describing the principle material directions is explained for solid elements for this material model. We will call the material direction the **a**-**b**-**c** coordinate system. The AOPT options illustrated in the AOPT figure of *MAT_002 can define the **a**-**b**-**c** system for all elements of the parts that use the material.

*EM_MAT_004

Purpose: Define the electromagnetic material type and properties for conducting shells in a 3D problem or in a 2D resistive heating problem.

*EM_**MAT_005**

Purpose: Used in applications that require two material conductivities per EM node and whose electromagnetic conductivities are defined by a (3*3) tensor matrix. Applications include Randles Batmac model and Electrophysiology Bidomain model.

Orthotropic Card 1.

Orthotropic Card 2.

Orthotropic Card 3.

Orthotropic Card 4.

Orthotropic Card 5.

Orthotropic Card 6.

matrix for the two conductivities.

Define AOPT for both options:

Remarks:

1.When this material is used in conjunction with the battery BatMac model, then the conductivities must be adjusted by the current collector thickness ratio over the total thickness of the cell. For example, if n_p is the number of positive current collectors, t_p the thickness of each individual positive current collector and Th the total thickness of the cell, then the conductivity for the positive current collector must be scaled by : $\frac{n_p \times t_p}{Th}$.

2.This card works in a similar way to *MAT_002 :

The procedure for describing the principle material directions is explained for solid elements for this material model. We will call the material direction the **a**-**b**-**c** coordinate system. The AOPT options illustrated in the AOPT figure of *MAT_002 can define the **a**-**b**-**c** system for all elements of the parts that use the material.
*EM_MAT_006

Purpose: Define two conductivities per EM node for special applications (Randles Batmac).

Remarks:

1. When this material is used in conjunction with the battery BatMac model, then the conductivities must be adjusted by the current collector thickness ratio over the total thickness of the cell. For example, if n_p is the number of positive current collectors, t_p the thickness of each individual positive current collector and ℎ the total thickness of the cell, then the conductivity for the positive current collector must be scaled by : $n_p \times t_p / \frac{n_p}{Th}$.

*EM_OUTPUT

Purpose: Define the level of EM related output on the screen and in the messag file.

Purpose: This keyword creates a set of points which can be used by the *EM_DATA-BASE_POINTOUT keyword.

Output Options Card.

Include as many cards as needed. This input ends at the next keyword ("*") card.

VARIABLE DESCRIPTION

VARIABLE DESCRIPTION POS Position flag (for 2D see Remark 1): EQ.0 (default) : The solver determines if the point is inside or outside of the conductors. EQ.1: Point outside of the conductors during the entire simulation. The solver does not check; hence a gain in computation time.

Remarks:

1. If using *EM_2DAXI notice that the conductors represents the corresponding 3D conductors.

*EM_RANDLES_BATMAC

Purpose: define the distributed Randles circuit parameters for a Randles cell when using the batmac model. The batmac model is a macro battery model where solid elements are retained for the solid mechanics and thermal solve and where each conducting node will have its own Randles circuit associated to it. Must be used with *EM_MAT_006 or *EM_MAT_005.

Optional Card. This card only needs to be defined for RDLTYPE greater than 1.

Optional thermal card.

Optional SOC shift card.

VARIABLE DESCRIPTION

RDLTYPE Type of Randles Cell:

EQ.-1: User defined equivalent circuit model. See Remark 3.

EQ.0: 0-order Randles Cell

EQ.1: 1-order Randles Cell

Remarks:

- 1. **Model combinations.** The batmac model cannot be mixed with the solid or thick shell Randles models. It can however be used in conjunction with the meshless model.
- 2. **Accounting for Diffusion Limitations.** Sometimes, an extra term called SOCshift (or SocS) can be added at high rate discharges to account for diffusion limitations. The SOCshift is added to SOC for the calculation of the OCV $u(SOC + SOC)$ and $r_0(SOC + SOC)$. SOCshift satisfies the following equation:

$$
\frac{d(\text{SOCshift})}{dt} + \frac{\text{SOCshift}}{\tau} = \frac{f(i(t))}{\tau}
$$

with SOCshift($t = 0$) = 0.

- 3. User defined ECMs. Randles circuits are based on the finite element Robin boundary condition, acting similarly to a convection boundary condition for the heat equation. As such, the circuit equation is decomposed into a term that will enter the left-hand-side of the stiffness matrix and a term that will be added to the right-hand-side. Changing the definition of those terms allows the user to replace the Randles circuits by any type of Equivalent Circuit model (ECM). This is the purpose of RDLTYPE=-1 where the term entering the l.h.s is defined by a negative integer referring to a *DEFINE_FUNCTION ID in R0CHA (unit consistency: Resistance) while a negative integer in R0DIS, associated to a *DEFINE_FUNCTION will give the term entering in the r.h.s (unit consistency : current).
- 4. **DEFINE FUNCTION**. Variables available in EM_RANDLES keywords for a *DEFINE_FUNCTION:

*EM_RANDLES_BATMAC *EM

*EM_**RANDLES_EXOTHERMIC_REACTION**

Purpose: This keyword allows the user to add an extra heat source term to the Randles circuit nodes in order to account for thermal runaway situations.

DESCRIPTION

- AREATYPE Works the same way as RDLAREA in *EM_RANDLES_SOLID or in *EM_RANDLES_TSHELL :
	- EQ.1: The heat source in FUNCTID is per unit area so that, for each local Randles circuit, the result returned by FUNC-TID is multiplied by a factor areaLoc (areaLoc is the local area associated to each Randles circuit while areaGlob is the area of the whole cell) ($W.m^2$).
	- EQ.2: Default. The heat source in FUNCTID is for the whole cell (the whole cell is shorted), so that, for each Randles circuit, the result returned by FUNCTID is multiplied by a factor areaLoc/areaGlob (W) .
	- EQ.3: The heat source returned by FUNCTID is taken as is in each Randles circuit (W).
- FUNCTID DEFINE_FUNCTION ID giving the local heat source function of local parameters for the local Randles circuit. See Remark 1.

Remarks:

1. **DEFINE FUNCTION** variables available in EM_RANDLES keywords :

*EM_RANDLES_EXOTHERMIC_REACTION *EM

*EM *EM_RANDLES_EXOTHERMIC_REACTION

*EM_RANDLES_MESHLESS

Purpose: define the distributed Randles circuit parameters for a Randles cell which is not associated with a mesh (lumped Randles circuit).

Optional Card. This card only needs to be defined for RDLTYPE greater than 1.

Thermal Optional card.

SOC shift Optional card.

VARIABLE DESCRIPTION

RDLID ID of the Randles Cell

Remarks:

1. Accounting for Diffusion Limitations. Sometimes, an extra term called SOCshift (or SocS) can be added at high rate discharges to account for diffusion limitations. The SOCshift is added to SOC for the calculation of the OCV $u(SOC + SOC)$ and $r_0(SOC + SOC)$. SOCshift satisfies the following equation:

$$
\frac{d(\text{SOCshift})}{dt} + \frac{\text{SOCshift}}{\tau} = \frac{f(i(t))}{\tau}
$$

with SOCshift($t = 0$) = 0.

- 2. **User defined ECMs.** Randles circuits are based on the finite element Robin boundary condition, acting similarly to a convection boundary condition for the heat equation. As such, the circuit equation is decomposed into a term that will enter the left-hand-side of the stiffness matrix and a term that will be added to the right-hand-side. Changing the definition of those terms allows the user to replace the Randles circuits by any type of Equivalent Circuit model (ECM). This is the purpose of RDLTYPE=-1 where the term entering the l.h.s is defined by a negative integer referring to a *DEFINE_FUNCTION ID in R0CHA (unit consistency: Resistance) while a negative integer in R0DIS, associated to a *DEFINE_FUNCTION will give the term entering in the r.h.s (unit consistency : current).
- 3. DEFINE FUNCTION. Variables available for *DEFINE_FUNTION in EM_- RANDLES keywords :

*EM_RANDLES_MESHLESS *EM

*EM_RANDLES_**TSHELL**

Purpose: Define the distributed Randles circuit parameters for a Randles cell when using a composite tshell mechanical model.

Card 3.b		$\overline{2}$	3	4	5	6		8
Variable	R20CHA	R ₂₀ DIS	C20CHA	C ₂₀ D _{IS}	R30CHA	R30DIS	C30CHA	C30DIS
Type	F	F	F	F	F	F	F	F
Default	0.	0.	0.	0.	0.	0.	0.	0.

Optional Card. This card only needs to be defined for RDLTYPE greater than 1.

Optional Thermal Card.

Optional SOCShift Card.

VARIABLE DESCRIPTION

RDLID ID of the Randles Cell

*EM *EM_RANDLES_TSHELL

*EM_RANDLES_TSHELL *EM

Remarks:

- 1. Sectioning of Circuit. Each part of PSID is defined by *PART_COMPOSITE_-TSHELL. With this keyword for defining the part, each layer of a part can serve a different function, namely, as a current collector positive, current collector negative, separator, negative electrode, or positive electrode. A given layer's function is defined in the RDLTYPE field of *EM_MAT_001.
- 2. **Accounting for Diffusion Limitations.** Sometimes, an extra term called SOCshift (or SocS) can be added at high rate discharges to account for diffusion limitations. The SOCshift is added to SOC for the calculation of the OCV $u(SOC + SOC)$ and $r_0(SOC + SOC)$. SOCshift satisfies the following equation:

$$
\frac{d(\text{SOCshift})}{dt} + \frac{\text{SOCshift}}{\tau} = \frac{f(i(t))}{\tau}
$$

with SOCshift($t = 0$) = 0.

- 3. **User defined ECMs**. Randles circuits are based on the finite element Robin boundary condition, acting similarly to a convection boundary condition for the heat equation. As such, the circuit equation is decomposed into a term that will enter the left-hand-side of the stiffness matrix and a term that will be added to the right-hand-side. Changing the definition of those terms allows the user to replace the Randles circuits by any type of Equivalent Circuit model (ECM). This is the purpose of RDLTYPE = -1 where the term entering the l.h.s is defined by a negative integer referring to a *DEFINE_FUNCTION ID in R0CHA (unit consistency: Resistance) while a negative integer in R0DIS, associated to a *DEFINE_FUNCTION will give the term entering in the r.h.s (unit consistency : current).
- 4. **DEFINE FUNCTION** variables available in EM_RANDLES keywords :

*EM_RANDLES_TSHELL *EM

*EM_**RANDLES_SHORT**

Purpose: For battery cell internal short, define conditions to turn on a Randles short (replace one or several Randles circuits by resistances), and to define the value of the short resistance.

Remarks:

1. If the return value of the function is zero, there is no short, the Randles circuit is maintained. A positive returned value will replace the Randles circuit by the returned short resistance. In order to ensure that the short is maintained even after the original criteria is no longer met, the default positive value may be

local parameters for the local Randles circuit. See Remark 2.

replaced by a negative value. The solver will then take the absolute value returned and adopt it as the new short resistance in case the original short criteria is no longer met rather than reverting to a Randles circuit.

2. The parameter description is :

3. An example of a function :

*DEFINE_FUNCTION

FID (Function Id)

Float resistance_short_randle(

float time,

float x_ccp,float y_ccp,float z_ccp,

float x_sep,float y_sep,float z_sep,

float x_sem,float y_sem,float z_sem,

float x_ccm,float y_ccm,float z_ccm)

{ float seThick0;

 $seThick0 = 1.e-5;$

 seThick=(sqrt(x_sep-x_sem)^2+(y_sep-y_sem)^2+(z_sep z _sem $)$ ^2);

if (seThick $>=$ seThick0) then

return -1.e-3;

else

return 1.e-2;

endif

In this example, as long as seThick is smaller than seThick0, no short occurs. Once seThick becomes larger than seThick0, a short occurs and the short resistance is 1.e-2. If during the run, seThick once again becomes smaller than seThick0, the short is maintained and the short resistance becomes 1.e-3. Replacing 1.e-3 by 0. would cause the short to revert to the original Randles circuit.

*EM_RANDLES_SOLID

Purpose: define the distributed Randles circuit parameters for a Randles cell when using a solid mechanical model.

Optional Card. This card only needs to be defined for RDLTYPE greater than 1.

Optional Thermal card.

Optional SOC shift card

VARIABLE DESCRIPTION

RDLTYPE Type of Randles Cell:

EQ.-1: User defined equivalent circuit model. See Remark 3.

- EQ.0: 0-order Randles Cell
- EQ.1: 1-order Randles Cell

Remarks:

- 1. Element Normal orientation. the solid element normals must all be oriented in the positive current collector to negative current collector direction in order to detect which current collector nodes are connected to one another. Furthermore, any number of layers can be modelled but the meshes of the CCP, anode, separator, cathode, CCN must be continuous and have merged nodes at the boundaries.
- 2. **Accounting for Diffusion Limitations.** Sometimes, an extra term called SOCshift (or SocS) can be added at high rate discharges to account for diffusion limitations. The SOCshift is added to SOC for the calculation of the OCV $u(SOC + SOC)$ and $r_0(SOC + SOC)$. SOCshift satisfies the following equation:

$$
\frac{d(\text{SOCshift})}{dt} + \frac{\text{SOCshift}}{\tau} = \frac{f(i(t))}{\tau}
$$

with SOCshift($t = 0$) = 0.

- 3. User defined ECMs. Randles circuits are based on the finite element Robin boundary condition, acting similarly to a convection boundary condition for the heat equation. As such, the circuit equation is decomposed into a term that will enter the left-hand-side of the stiffness matrix and a term that will be added to the right-hand-side. Changing the definition of those terms allows the user to replace the Randles circuits by any type of Equivalent Circuit model (ECM). This is the purpose of RDLTYPE=-1 where the term entering the l.h.s is defined by a negative integer referring to a *DEFINE_FUNCTION ID in R0CHA (unit consistency: Resistance) while a negative integer in R0DIS, associated to a *DEFINE_FUNCTION will give the term entering in the r.h.s (unit consistency : current).
- 4. **DEFINE FUNCTION.** Variables available in EM_RANDLES keywords for *DE-FINE_FUNCTION:

*EM_ROTATION_AXIS

Purpose: Define a rotation axis for the EM solver. This is used with the 2D axisymmetric solver. The axis is defined by a point and a direction.

VARIABLE DESCRIPTION

 XP, YP, ZP , x, y, and z coordinates of the point

 XD, YD, ZD $x, y,$ and z components of direction of the axis

NUMSEC Number of Sectors. This field gives the ratio of the full circle to the angular extension of the mesh. This has to be a power of two. For example, NUMSEC $=$ 4 means that the mesh of the part represents one fourth of the total circle. If NUMSEC = 0 for [*EM_2DAXI,](#page-201-0) the solver will replace it with this value.

*EM_SOLVER_BEM

Purpose: Define the type of linear solver and pre-conditioner as well as tolerance for the EM_BEM solve.

Remarks:

- 1. **USELAST.** Using USELAST = 1 can save many iterations in the subsequent solves if the vector solution of the present solve is assumed to be nearly parallel to the vector solution of the previous solve, as usually happens in timedomain eddy-current problems.
- 2. **Moving Conductors.** Since the BEM matrices depend on (and only on) the surface node coordinates of the conductors, it is important to recalculate them when the conductors are moving. The frequency with which they are updated is controlled by NCYLBEM. Note that very small values, for example NCYL-BEM = 1, should, generally, be avoided since this calculation involves a high computational cost. However, when two conductors are moving and in contact with each other it is recommended to recalculate the matrices at *every* time step.

*EM_SOLVER_BEMMAT

Purpose: Define the type of BEM matrices as well as the way they are assembled.

*EM_SOLVER_FEM

Purpose: Define some parameters for the EM FEM solver.

Remarks:

- 1. Starting from Previous Solution. Using USELAST $= 1$ can save many iterations in the subsequent solves if the vector solution of the present solve is assumed to be nearly parallel to the vector solution of the previous solve, as usually happens in time-domain eddy-current problems.
- 2. Default Values. The default values are only valid when the PCG resolution method (STYPE = 2) is used. For the default direct solve (STYPE = 1), those values are ignored.
- 3. **NCYCLFEM.** When the conductor parts are deforming or undergoing changes in their EM material properties (conductivity for example), the FEM matrices should be recalculated more often, so NCYCLFEM may need to be changed.

*EM_SOLVER_FEMBEM

Purpose: Define some parameters for the coupling between the EM_FEM and EM_BEM solvers.

Remarks:

1. **STYPE.** For the default Richardson method, at each time step, the solver will iterate between the FEM and the BEM system until reaching convergence (based on the choice of RELTOL and MAXITER). The cost for this solve is low. However, in order to ensure stability, we recommend imposing a limit on the timestep based on the characteristic diffusion time (See *EM_CONTROL_- TIMESTEP). Furthermore, it can be unstable whenever magnetic materials are involved (conductor's permeability different than vacuum permeability). The

monolithic solver on the other hand aims to remove those two limitations by solving both the FEM and BEM systems in one single monolithic bloc. For such cases, it is, therefore, the recommended choice.

*ICFD

The keyword *ICFD covers all the different options available in the incompressible fluid solver. The keyword cards in this section are defined in alphabetical order:

*ICFD_BOUNDARY_CONJ_HEAT

*ICFD_BOUNDARY_CONVECTION_TEMP

*ICFD_BOUNDARY_FLUX_TEMP

*ICFD_BOUNDARY_FREESLIP

*ICFD_BOUNDARY_FSI

*ICFD_BOUNDARY_FSI_EXCLUDE

*ICFD_BOUNDARY_FSWAVE

*ICFD_BOUNDARY_GROUND

*ICFD_BOUNDARY_NONSLIP

*ICFD_BOUNDARY_PERIODIC

*ICFD_BOUNDARY_PRESCRIBED_MOVEMESH

*ICFD_BOUNDARY_PRESCRIBED_PRE

*ICFD_BOUNDARY_PRESCRIBED_TEMP

*ICFD_BOUNDARY_PRESCRIBED_TURBULENCE

*ICFD_BOUNDARY_PRESCRIBED_VEL

*ICFD_BOUNDARY_WINDKESSEL

*ICFD_CONTROL_ADAPT

*ICFD_CONTROL_ADAPT_SIZE

*ICFD_CONTROL_CONJ

*ICFD_CONTROL_DEM_COUPLING

*ICFD_CONTROL_EMBEDSHELL

*ICFD_CONTROL_FSI

*ICFD

*ICFD_CONTROL_GENERAL *ICFD_CONTROL_IMPOSED_MOVE *ICFD_CONTROL_LOAD *ICFD_CONTROL_MESH *ICFD_CONTROL_MESH_MOV *ICFD_CONTROL_MONOLITHIC *ICFD_CONTROL_OUTPUT *ICFD_CONTROL_OUTPUT_SUBDOM *ICFD_CONTROL_OUTPUT_VAR *ICFD_CONTROL_PARTITION *ICFD_CONTROL_POROUS *ICFD_CONTROL_STEADY *ICFD_CONTROL_SURFMESH *ICFD_CONTROL_TAVERAGE *ICFD_CONTROL_TIME *ICFD_CONTROL_TRANSIENT *ICFD_CONTROL_TURB_SYNTHESIS *ICFD_CONTROL_TURBULENCE *ICFD_DATABASE_AVERAGE *ICFD_DATABASE_DRAG *ICFD_DATABASE_FLUX *ICFD_DATABASE_HTC *ICFD_DATABASE_NODEAVG *ICFD_DATABASE_NODOUT

*ICFD_DATABASE_POINTAVG

*ICFD_DATABASE_POINTOUT

*ICFD_DATABASE_RESIDUALS

*ICFD_DATABASE_TEMP

*ICFD_DATABASE_TIMESTEP

*ICFD_DATABASE_UINDEX

*ICFD_DEFINE_HEATSOURCE

*ICFD_DEFINE_NONINERTIAL

*ICFD_DEFINE_POINT

*ICFD_DEFINE_SOURCE

*ICFD_DEFINE_TURBSOURCE

*ICFD_DEFINE_WAVE_DAMPING

*ICFD_INITIAL

*ICFD_INITIAL_LEVELSET

*ICFD_INITIAL_TURBULENCE

*ICFD_MAT

*ICFD_MODEL_NONNEWT

*ICFD_MODEL_POROUS

*ICFD_PART

*ICFD_PART_VOL

*ICFD_SECTION

*ICFD_SET_NODE

*ICFD_SOLVER_SPLIT

*ICFD_SOLVER_TOL_FSI

*ICFD_SOLVER_TOL_LSET

*ICFD_SOLVER_TOL_MMOV

*ICFD_SOLVER_TOL_MOM

*ICFD_SOLVER_TOL_MONOLITHIC

*ICFD_SOLVER_TOL_PRE

*ICFD_SOLVER_TOL_TEMP

*ICFD_BOUNDARY_CONJ_HEAT

Purpose: Specify which boundary of the fluid domain will exchange heat with the solid.

Include as many cards as needed. This input ends at the next keyword ("*") card.

*ICFD_BOUNDARY_**CONVECTION**_TEMP

Purpose: Impose a heat transfer coefficient on the boundary expressed as $h = \frac{q}{T_s - T_b}$

Include as many cards as needed. This input ends at the next keyword ("*") card.

VARIABLE DESCRIPTION

- PID **PID** for a fluid surface.
- HLCID Load curve ID to describe the heat transfer coefficient value versus time, see *DEFINE_CURVE,*DEFINE_CURVE_FUNC-TION or *DEFINE_FUNCTION. If a DEFINE_FUNCTION is used, the following parameters are allowed: $f(x, y, z, vx, vy, vz, temp, pres, time).$
- HSF Load curve scale factor applied on the heat transfer coefficient value. (default $= 1.0$)
- TBLCID Load curve ID to describe the environment (i.e bulk) temperature value versus time, see *DEFINE_CURVE,*DEFINE_CURVE_- FUNCTION or *DEFINE_FUNCTION. If a DEFINE_FUNCTION is used, the following parameters are allowed: $f(x, y, z, vx, vy, vz, temp, pres, time).$
	- TBSF Load curve scale factor applied on the environment value. $(default = 1.0)$

*ICFD_BOUNDARY_FLUX_TEMP

Purpose: Impose a heat flux on the boundary expressed as $q = -k\nabla T$

Include as many cards as needed. This input ends at the next keyword ("*") card.

DESCRIPTION

SF Load curve scale factor. (default = 1.0)

- DEATH Time at which the imposed motion/constraint is removed: EQ.0.0: default set to 10e28
- BIRTH Time at which the imposed pressure is activated starting from the initial abscissa value of the curve

*ICFD_BOUNDARY_FREESLIP

Purpose: Specify the fluid boundary with free-slip boundary condition.

Include as many cards as needed. This input ends at the next keyword ("*") card.

VARIABLE DESCRIPTION

PID PID of the fluid surface where a free-slip boundary condition is applied.

*ICFD_BOUNDARY_FSI

Purpose: This keyword defines which fluid surfaces will be considered in contact with the solid surfaces for fluid-structure interaction (FSI) analysis. This keyword should not be defined if *ICFD_CONTROL_FSI is not defined.

Include as many cards as needed. This input ends at the next keyword ("*") card.

VARIABLE DESCRIPTION

PID PID of the fluid surface in contact with the solid domain.

*ICFD_BOUNDARY_FSI_EXCLUDE

Purpose: This keyword defines which solid part IDs are excluded from the FSI search. No forces coming from the fluid will be transmitted on those parts.

Include as many cards as needed. This input ends at the next keyword ("*") card.

VARIABLE DESCRIPTION

PID Part ID of the solid mechanics problem which is to be excluded from the FSI analysis.

*ICFD_BOUNDARY_**FSWAVE**

Purpose: Impose a wave inflow boundary condition.

VARIABLE DESCRIPTION

WANG Angle between incoming wave direction and x-axis for z and yaligned gravity vector, or angle between incoming wave direction and y-axis for x-aligned gravity vector.

*ICFD_BOUNDARY_GROUND

Purpose: Specify the fluid boundary with a ground boundary condition. The ground boundary condition is similar to the nonslip boundary condition except that it will keep $V = 0$ in all circumstances, even if the surface nodes are moving. This is useful in cases where the nodes are allowed to move or translate (using ICFD_BOUNDARY_PRE-SCRIBED_MOVEMESH for example) but those displacements are only to accommodate for mesh movement and do not correspond to a physical motion.

Include as many cards as needed. This input ends at the next keyword ("*") card.

VARIABLE DESCRIPTION

PID PID of the fluid surface where a ground boundary condition is applied.

*ICFD_BOUNDARY_NONSLIP

Purpose: Specify the fluid boundary with a non-slip boundary condition.

Include as many cards as needed. This input ends at the next keyword ("*") card.

VARIABLE DESCRIPTION

PID PID of the fluid surface where a non-slip boundary condition is applied.

*ICFD_BOUNDARY_**PERIODIC**

Purpose: Allows the user to impose various kind of constraints between two fluid surfaces.

ANGLE Rotation angle for PTYPE = 1. Characterizes contact distance for $PTYPE = 3$ and axe different then 0.

Remarks:

1. Selection of master PID. When the two meshes are of different densities, it is recommended to select the finer mesh as PID and the coarser as PID2.

*ICFD_BOUNDARY_PRESCRIBED_MOVEMESH

Purpose: Allows the node of a fluid surface to translate in certain directions using an ALE approach. This is useful in piston type applications or can also be used in certain cases to avoid big mesh deformation.

Include as many cards as needed. This input ends at the next keyword ("*") card.

*ICFD_BOUNDARY_PRESCRIBED_PRE

Purpose: Impose a fluid pressure on the boundary.

VARIABLE DESCRIPTION

*ICFD_BOUNDARY_PRESCRIBED_TEMP

Purpose: Impose a fluid temperature on the boundary.

Include as many cards as needed. This input ends at the next keyword ("*") card.

*ICFD_BOUNDARY_PRESCRIBED_TURBULENCE

Purpose: Optional keyword that allows the user to strongly impose the turbulence quantities when a RANS turbulence model is selected. See ICFD_CONTROL_TURBU-LENCE. Mainly used to modify the default boundary conditions at the inlet.

Include as many cards as needed. This input ends at the next keyword ("*") card.

Remarks:

1. At the inlet, the relationship between the turbulent kinetic energy k and the turbulence intensity I is given by :

$$
k=\frac{3}{2}(U_{avg}^2I^2)
$$

By default, the solver uses an inlet intensity of 0.05 (5%).

2. At the inlet, if specifying the turbulent dissipation rate using a length scale, l , the following relationship will be used :

$$
\epsilon = C_{\mu}^{3/4} \frac{k^{3/2}}{l}
$$

By default, the solver estimates a length scale based on the total height of the channel. Otherwise, if using the turbulent viscosity ratio $r = \frac{\mu_t}{\mu}$ method:

$$
\epsilon = \rho C_{\mu} \frac{k^2}{\mu r}
$$

3. At the inlet, if specifying the specific dissipation rate using a length scale, l , the following relationship will be used :

$$
\omega = C_{\mu}^{-1/4} \frac{k^{1/2}}{l}
$$

By default, the solver estimates a length scale based on the total height of the channel. Otherwise, if using the turbulent viscosity ratio $r = \frac{\mu_t}{\mu}$ method:

$$
\omega = \rho \frac{k}{\mu r}
$$

4. At the inlet, the relationship between the modified turbulent viscosity \tilde{v} is given and the length scale, l is given by :

$$
\tilde{\nu}=0.05\sqrt{\frac{3}{2}}\,(U_{avg}\,l)
$$

*ICFD_BOUNDARY_PRESCRIBED_VEL

Purpose: Impose the fluid velocity on the boundary.

*ICFD_**BOUNDARY_WINDKESSEL**

Purpose: This boundary condition imposes the pressure function of circuit parameters where an analogy is made between the pressure and scalar potential as well as between the flux and the current intensity. Such conditions are frequently encountered in hemodynamics.

Optional card if WTYPE = 3 or 4.

VARIABLE DESCRIPTION

Figure [1]. Windkessel circuit

Remarks:

1. Figure 1 shows a Windkessel circuit and Figure 2 a CV circuit.

Figure [2]. CV Circuit

*ICFD_CONTROL_ADAPT

Purpose: This keyword will activate the adaptive mesh refinement feature. The solver will use an a-posteriori error estimator to compute a new mesh size bounded by the user to satisfy a maximum perceptual global error.

VARIABLE DESCRIPTION

- KIS Keep initial mesh size:
	- EQ.0: Turned Off. The remeshing process will ignore the initial mesh size in the volume.
	- EQ.1: Turned on. Whenever a remeshing occurs, the new local mesh size will not be allowed to be substantially coarser than the one from the previous mesh. The object is to diminish the excessive coarsening that can occur between two remeshes.

*ICFD_CONTROL_ADAPT_SIZE

Purpose: This keyword controls the re-meshing of elements taking into account the element quality and distortion in contrast to the default algorithm which only checks for inverted elements.

*ICFD_CONTROL_**CONJ**

Purpose: This keyword allows to pick between the different coupling methods for conjugate heat transfer applications

VARIABLE DESCRIPTION

CTYPE Indicates the thermal coupling type.

- EQ.0: Robust and accurate monolithic coupling where the temperature field are solved simultaneously between the fluid and the structure.
- EQ.1: Weak thermal coupling. The fluid passes the heat flux to the solid at the fluid-structure interface and the solid returns the temperature which is applied as a Dirichlet condition.
- TSF Thermal Speedup Factor. This factor multiplies all thermal parameters present in the heat equation with units of time in the denominator (e.g., thermal conductivity, convection heat transfer coefficients). It is used to artificially time scale the thermal problem. A negative value will refer to a time dependent load curve.

Remarks:

1.The keyword ICFD_BOUNDARY_CONJ_HEAT is ignored if CTYPE = 1 but the keyword ICFD_BOUNDARY_FSI is needed in all thermal coupling cases.

*ICFD_CONTROL_DEM_COUPLING

Purpose: This keyword is needed to activate coupling between the ICFD and DEM solvers.

Remarks:

1. Morrison's formula. Morrison's formula for C_d calculation:

$$
C_d = \frac{24}{\text{Re}} + \frac{2.6 \left(\frac{\text{Re}}{5}\right)}{1 + \left(\frac{\text{Re}}{5}\right)^{1.52}} + \frac{0.411 \left(\frac{\text{Re}}{2.63 \times 10^5}\right)^{-7.94}}{1 + \left(\frac{\text{Re}}{2.63 \times 10^5}\right)^{-8.00}} + \frac{0.25 \left(\frac{\text{Re}}{10^6}\right)}{1 + \left(\frac{\text{Re}}{10^6}\right)}
$$

*ICFD_CONTROL_**EMBEDSHELL**

Purpose: This keyword allows the user to control specific options related to the use of the keyword MESH_EMBEDSHELL.

*ICFD_CONTROL_FSI

Purpose: This keyword modifies default values for the fluid-structure interaction coupling algorithm.

VARIABLE DESCRIPTION

Figure 0-1. Geometry of FSI contact.

Remarks:

1. Detecting Fluid-Solid Interaction. One of the criteria to automatically detect the fluid and solid surfaces that will interact in FSI problems is the distance d between a fluid (solid) node and a solid (fluid) element, respectively:

$$
d \leq \text{IDC} \times \min(h, H) ,
$$

where h is the size of the fluid mesh, H is the size of the solid mechanics mesh, and IDC is a detection coefficient criteria with IDC = 0.25 by default. In the majority of cases, this default value is sufficient to ensure FSI interaction. However, it can happen in special cases that the fluid and solid geometries have curvatures that differ too much (such as pipe flows in conjugate heat transfer applications). In such cases, a bigger IDC value may be needed. This flag should be handled with care.

2. **Rotation and Projection of Nodes.** $XPROJ = 1$ is recommended for cases with rotation.

*ICFD_CONTROL_**GENERAL**

Purpose: This keyword allows choosing between the different types of CFD analyses.

*ICFD_CONTROL_IMPOSED_MOVE

Purpose: This keyword allows the user to impose a velocity on specific ICFD parts or on the whole volume mesh. Global translation, global rotation and local rotation components can be defined and combined. This can be used in order to save calculation time in certain applications such as sloshing where the modeling of the whole fluid box and the solving of the consequent FSI problem is not necessarily needed.

Optional Card. Local reference frame definition if ALPHAL, BETAL or GAMMAL used.

Remarks:

Figure 7-1. A rotation represented by Euler angles (α, β, γ) using $\mathbf{Z}(\alpha)\mathbf{X}(\beta)\mathbf{Z}(\gamma)$ intrinsic rotations.

1. **Rotations.** Any target orientation can be reached starting from a known reference orientation using a specific sequence of intrinsic rotations whose magnitudes are the Euler angles (α, β, γ) . Equivalently, any rotation matrix R can be decomposed as a product of three elemental rotation matrices. For instance:

$$
\mathbf{R} = \mathbf{X}(\alpha) \mathbf{Y}(\beta) \mathbf{Z}(\gamma)
$$

However, different definition of the elemental rotation matrices (x, y, z) and their multiplication order can be adopted. The ICFD solver uses the following approach and rotation matrix:

$$
\mathbf{Z}(\alpha)\mathbf{X}(\beta)\mathbf{Z}(\gamma) = \begin{bmatrix} c_{\alpha}c_{\gamma} - c_{\beta}s_{\alpha}s_{\gamma} & -c_{\beta}c_{\gamma}s_{\alpha} - c_{\alpha}s_{\gamma} & s_{\alpha}s_{\beta} \\ c_{\gamma}s_{\alpha} + c_{\alpha}c_{\beta}s_{\gamma} & c_{\alpha}c_{\beta}c_{\gamma} - s_{\alpha}s_{\gamma} & -c_{\alpha}s_{\beta} \\ s_{\beta}s_{\gamma} & c_{\gamma}s_{\beta} & c_{\beta} \end{bmatrix}
$$

where $X(\alpha)$, $Y(\beta)$, and $Z(\gamma)$ *are* the matrices representing the elemental rotations about the axes (x, y, z) , $s_\alpha = \sin(\alpha)$, and $c_\beta = \cos(\beta)$.

2. Local Coordinate Systems. It is possible to have the ICFD parts or ICFD_-PART_VOLs rotate around the global reference frame but also to define and use a local reference frame by defining its point of origin and two of its vectors $\mathbf{v}_1 = (X1, Y1, Z1)$ and $\mathbf{v}_2 = (X2, Y2, Z2)$. The third vector is, then, in the direction of $\mathbf{v}_1 \times \mathbf{v}_2$. See [Figure 7-1.](#page-379-2)

*ICFD_CONTROL_LOAD

Purpose: This keyword resets the body load in the ICFD solver to zero, while leaving the body load unchanged for the solid mechanics solver. It is useful in problems where the gravity acceleration may be neglected for the fluid problem, but not for the solid mechanics problem.

VARIABLE DESCRIPTION

ABL EQ.0: the body load provided in *LOAD_BODY is reset to zero only for the fluid analysis.

*ICFD_CONTROL_MESH

Purpose: This keyword modifies default values for the automatic volume mesh generation.

Remarks:

1. For MGSF, values between 1 and 2 are allowed. Values closer to 1 will result in a finer volume mesh (1 means the volume mesh is not allowed to be coarser than the element size from the closest surface meshes) and values closer to 2 will result in a coarser volume mesh (2 means the volume can use elements as

much as twice as coarse as those from the closest surface mesh). MGSF has a fixed value of 1 in 2D.

- 2. If the user knows in advance that no remeshing will occur during the analysis, then setting NRMSH to 1may be useful as it will free space used to back up the mesh and consequently lower memory consumption.
- 3. The Default Mesh generation strategy (based on Delaunay criteria) yields a linear interpolation of the mesh size between two surfaces facing each other whereas the octree based generation strategy allows for elements' sizes to remain close to the element surface mesh size over a longer distance. This can be useful in configurations where two surface meshes facing each other have very distinct sizes in order to create a smoother transition.

*ICFD_CONTROL_MESH_MOV

Purpose: With this keyword the user can choose the type of algorithm for mesh movement.

*ICFD_CONTROL_**MONOLITHIC**

Purpose: This keyword allows to choose between the Fractional Step Solver and the Monolithic Solver.

VARIABLE DESCRIPTION

SID Solver ID :

EQ.0: Fractional Step Solver. Default.

EQ.1: Monolithic Solver.

*ICFD_CONTROL_OUTPUT

Purpose: This keyword modifies default values for screen and file outputs related to this fluid solver only.

VARIABLE DESCRIPTION

MSGL Message level.

EQ.0: only time step information is output.

EQ.1: first level solver information.

EQ.2: full output information with details about linear algebra and convergence steps.

EQ.4: full output information is also copied to the messag file.

.

GENERAL).

*ICFD_CONTROL_OUTPUT_SUBDOM

Purpose: Defines a specific zone that should be output in the format specified by the ICFD_CONTROL_OUTPUT card rather than the whole domain.

Shape Control. First card specifies the shape of the output sub domain.

Box Case. Card 2 for Sname = box

Sphere Case. Card 2 for Sname = sphere

*ICFD_CONTROL_OUTPUT_SUBDOM *ICFD

Cylinder Case. Card 2 for Sname = cylinder

*ICFD_CONTROL_OUTPUT_VAR

Purpose: This keyword allows the user to turn off the output of certain CFD variables to reduce the size of the d3plot files.

.

*ICFD_CONTROL_PARTITION

Purpose: This keyword changes the default option for the partition in MPP, thus it is only valid in MPP.

VARIABLE DESCRIPTION

PTECH Indicates the type of partition:

EQ.1: the library Metis is used.

EQ.2: partition along the axis with higher aspect ratio

EQ.3: partition along X -axis

EQ.4: partition along Y -axis

EQ.5: partition along Z -axis

*ICFD_CONTROL_**POROUS**

Purpose: This keyword modifies the porous media solve.

VARIABLE DESCRIPTION

PMSTYPE Indicates the porous media solve type.

- EQ.0: Anisotropic Generalized Navier-Stokes model for porous media (See *ICFD_MODEL_POROUS) using Fractional step method.
- EQ.1: Anisotropic Darcy-Forcheimer model using a Monolithic approach for the solve. This method is better suited for very low Reynolds flows through porous media (Frequently encountered in Resin Transfer Molding (RTM) applications).

Remarks:

1. When using the Anisotropic Darcy-Forcheimer model, the convective term in the Navier Stokes formulation is neglected.

*ICFD_CONTROL_**STEADY**

Purpose: This keyword allows to specify convergence options for the steady state solver.

*ICFD_CONTROL_SURFMESH

Purpose: This keyword enables automatic surface re-meshing. The objective of the remeshing is to improve the mesh quality on the boundaries. It should not be used on a regular basis.

.

*ICFD_CONTROL_**T**AVERAGE

Purpose: This keyword controls the restarting time for computing the time average values. By default, there is no restarting and the average quantities are given starting from $t = 0$. This keyword can be useful in turbulent problems that admit a steady state.

VARIABLE DESCRIPTION

DT Over each DT time interval, the average quantities are reset.
*ICFD_CONTROL_TIME

Purpose: This keyword is used to change the defaults related to time parameters in the fluid problem.

TDEATH Death time for the Navier Stokes solve. After TDEATH, the velocity and pressure will no longer be updated. But the temperature and other similar quantities still can.

*ICFD_CONTROL_**TRANSIENT**

Purpose: This keyword allows to specify different integration scheme options for the transient solver.

*ICFD_CONTROL_TURBULENCE

Purpose: Modify the default values for the turbulence model.

Card Summary:

[Card 1.](#page-399-0) This card is required.

[Card 2a.](#page-401-0) This card is read if $TMOD = 1$. It is optional.

[Card 2b.](#page-401-1) This card is read if TMOD = 2 or 3. It is optional.

[Card 2c.1.](#page-402-0) This card is read if $TMOD = 4$. It is optional.

[Card 2c.2.](#page-402-1) This card is read if $TMOD = 4$. It is optional.

[Card 2d.](#page-403-0) This card is read if $TMOD = 5$. It is optional.

Data Card Definitions:

VARIABLE DESCRIPTION

TMOD Indicates what turbulence model will be used.

EQ.1: Thermal law of the wall

TYPLUS Thermal Y+ value (Y_{+t}) . If Y_{+t} is not defined, the solver will automatically estimate its value using $Y_{+tc} = Y_{+c} / \text{Pr}^{1./3.}$ with $Y_{+c} = 11.225$ the critical Y_+ value and Pr the Prandtl number.

RANS $k - \varepsilon$ **Card. Optional card if TMOD = 1.** Optional card read if TMOD = 1. See [Remark 1.](#page-403-1)

Card 2a		$\overline{2}$	3	4	5	6	8
Variable	CE ₁	CE ₂	SIGMAE	SIGMAK	CMU	CCUT	
Type	F	F	F	F	F	F	
Default	1.44	1.92	1.3	1.0	0.09	-1.	

VARIABLE DESCRIPTION

LES Card. Optional card read if $TMOD = 2$ or 3.

Cs Smagorinsky constant if TMOD = 2 and SUBMOD = 1 or WALE constant if $TMOD = 3$

RANS $k - \omega$ **Card.** Optional card read if TMOD = 4. See [Remark 2.](#page-404-0)

Card 2c.1		$\overline{2}$	3	4	5	6	8
Variable	GAMMA	BETA01	SIGMAW1	SIGMAK1	BETA0ST	CCUT	
Type	F.	F	F	F	F	F	
Default	1.44	0.072	2.	2.	0.09	-1.	

RANS $k - \omega$ **Card.** Optional card read if TMOD = 4. See [Remark 2.](#page-404-0)

- SIGMAK2 $k \omega$ model constant, σ_{k2}
	- CL $k \omega$ model constant, C_l

RANS Spalart-Allmaras Card. Optional card read if TMOD = 5.

Remarks:

1. $k - \varepsilon$ **Model (TMOD = 1).** For the Standard $k - \varepsilon$ model, the following two equations are solved for the turbulent kinetic energy (k) and the turbulent dissipation (ε) :

$$
\frac{\partial k}{\partial t} + \frac{\partial (ku_i)}{\partial x_i} = \frac{\partial}{\partial x_j} \left[\left(\frac{\mu}{\rho} + \frac{\mu_t}{\rho \sigma_k} \right) \frac{\partial k}{\partial x_j} \right] + P_k + P_b - \varepsilon + S_k
$$

$$
\frac{\partial \varepsilon}{\partial t} + \frac{\partial (\varepsilon u_i)}{\partial x_i} = \frac{\partial}{\partial x_j} \left[\left(\frac{\mu}{\rho} + \frac{\mu_t}{\rho \sigma_{\varepsilon}} \right) \frac{\partial \varepsilon}{\partial x_j} \right] + C_{1\varepsilon} \frac{\varepsilon}{k} P_k - C_{2\varepsilon} \frac{\varepsilon^2}{k} + S_e
$$

Here P_k is the k production term (see [Remark 3\)](#page-406-1), P_b is the production term due to buoyancy and S_k and S_e are the user defined source terms. P_k and P_b are expressed as:

$$
P_k = \frac{\mu_t}{\rho} S^2
$$

$$
P_b = \frac{\beta \mu_t}{\rho Pr_t} g_i \frac{\partial T}{\partial x_i}
$$

where *S* is the modulus of the mean rate of strain tensor ($S^2 = 2S_{ij}S_{ij}$), β is the coefficient of thermal expansion, and Pr_t is the turbulent Prandtl number. The turbulent viscosity is then expressed as:

$$
\mu_t = \rho C_\mu \frac{k^2}{\varepsilon}
$$

For the realizable k - ε model, the equation for the turbulent kinetic energy does not change, but the equation for the turbulent dissipation is now expressed as:

$$
\frac{\partial \varepsilon}{\partial t} + \frac{\partial (\varepsilon u_i)}{\partial x_i} = \frac{\partial}{\partial x_j} \left[\left(\frac{\mu}{\rho} + \frac{\mu_t}{\rho \sigma_{\varepsilon}} \right) \frac{\partial \varepsilon}{\partial x_j} \right] + C_1 S \varepsilon - C_{2\varepsilon} \frac{\varepsilon^2}{k + \sqrt{\frac{\mu}{\rho} \varepsilon}} - \varepsilon + S_{\varepsilon}.
$$

Here $C_1 = \max\left[0.43, \frac{\eta}{\eta+5}\right]$ with $\eta = S\frac{k}{\varepsilon}$.

Furthermore, while the turbulent viscosity is still expressed the same way, C_{μ} is no longer a constant:

$$
C_{\mu} = \frac{1}{A_0 + A_s k \frac{U^*}{\epsilon}}.
$$

In the above,

$$
U^* = \sqrt{\Omega_{ij}\Omega_{ij} + S_{ij}S_{ij}}
$$

\n
$$
A_0 = 4.04
$$

\n
$$
A_s = \sqrt{6}\cos\left(\frac{1}{3}\cos^{-1}\left(\sqrt{6}\frac{S_{ij}S_{jk}S_{ki}}{(S_{ij}S_{ij})^{3/2}}\right)\right)
$$

Note that in this case, the constant value C_{μ} that can be input by you serves as the limiting value that C_{μ} can take. By default, $C_{\mu} = 0.09$ so:

$$
0.0009 < C_{\mu} < 0.09
$$

2. $k - \omega$ **Model (TMOD = 4).** For the Standard Wilcox 06 $k - \omega$ model, the following two equations are solved for the turbulent kinetic energy and the specific turbulent dissipation rate, respectively k and ω :

$$
\frac{\partial k}{\partial t} + \frac{\partial (ku_i)}{\partial x_i} = \frac{\partial}{\partial x_j} \left[\left(\frac{\mu}{\rho} + \frac{\mu_t}{\rho \sigma_{k1}} \right) \frac{\partial k}{\partial x_j} \right] + P_k - \beta^* k \omega + S_k
$$

$$
\frac{\partial \omega}{\partial t} + \frac{\partial (\omega u_i)}{\partial x_i} = \frac{\partial}{\partial x_j} \left[\left(\frac{\mu}{\rho} + \frac{\mu_t}{\rho \sigma_{\omega 1}} \right) \frac{\partial \varepsilon}{\partial x_j} \right] + \gamma \frac{\omega}{k} P_k - \beta \omega^2 + \sigma_d X_k \omega^2 + S_\omega
$$

Here P_k is the k production term (see [Remark 3\)](#page-406-1) and S_k and S_ω are the user defined source terms. P_k , β^* , β and σ_d are expressed as:

$$
P_k = \frac{\mu_t}{\rho} S^2
$$

\n
$$
\beta^* = \beta_0^* f_{\beta*}
$$

\n
$$
\beta = \beta_0 f_{\beta}
$$

\n
$$
\sigma_d = \begin{cases} 0. & X_k \le 0. \\ 1/8 & X_k > 0. \end{cases}
$$

where

$$
f_{\beta} = \frac{1 + 85X_{\omega}}{1 + 100X_{\omega}}
$$

$$
f_{\beta*} = 1.
$$

$$
X_k = \frac{1}{\omega^3} \frac{\partial k}{\partial x_j} \frac{\partial \omega}{\partial x_j}
$$

$$
X_{\omega} = \frac{\left| \Omega_{ij} \Omega_{jk} S_{ki} \right|}{\left(\beta_0^* \omega \right)^3}
$$

The turbulent viscosity is then:

$$
\mu_t = \rho \frac{k}{\max\left[\omega, C_l \sqrt{\frac{2S_{ij}S_{ij}}{\beta_0^*}}\right]}
$$

For the Standard Wilcox 98 model, the following terms are modified:

$$
f_{\beta} = \frac{1 + 70X_{\omega}}{1 + 80X_{\omega}}
$$

\n
$$
f_{\beta*} = \begin{cases} 1 & \text{if } X_k \le 0. \\ \frac{1 + 680 X_k^2}{1 + 400 X_k^2} & \text{if } X_k > 0. \end{cases}
$$

\n
$$
\sigma_d = 0.
$$

The turbulent viscosity is then:

$$
\mu_t = \rho \frac{k}{\omega}
$$

For the Menter SST 2003 model, the following equations are solved:

$$
\frac{\partial k}{\partial t} + \frac{\partial (ku_i)}{\partial x_i} = \frac{\partial}{\partial x_j} \left[\left(\frac{\mu}{\rho} + \frac{\mu_t}{\rho \sigma_k} \right) \frac{\partial k}{\partial x_j} \right] + P_k - \beta_0^* k \omega + S_k
$$

$$
\frac{\partial \omega}{\partial t} + \frac{\partial (\omega u_i)}{\partial x_i} = \frac{\partial}{\partial x_j} \left[\left(\frac{\mu}{\rho} + \frac{\mu_t}{\rho \sigma_\omega} \right) \frac{\partial \varepsilon}{\partial x_j} \right] + \frac{\gamma}{\mu_t} P_k - \beta \omega^2 + 2(1 - F_1) \sigma_{\omega 2} X_k \omega^2 + S_\omega
$$

Each of the constants, γ , β , σ_k , and σ_ω are now computed by a blend of two constants with a blending function through:

$$
\alpha = \alpha_1 F_1 + \alpha_2 (1 - F_1)
$$

The blending function F_1 is defined by:

$$
F_1 = \tanh\left\{\left[\min\left(\max\left(\frac{\sqrt{k}}{\beta_0^* \omega y}, \frac{500\nu}{y^2 \omega}\right), \frac{4\rho \sigma_{\omega 2} k}{CD \times y^2}\right)\right]^4\right\}
$$

With y the distance to the nearest wall and:

$$
CD = \max(2\rho \sigma_{\omega 2} X_k \omega^2, 10^{-10})
$$

The turbulent viscosity is then:

$$
\mu_t = \rho \frac{a_1 k}{\max(a_1 \omega, S F_2)}
$$

with:

$$
F_2 = \tanh\left[\left(\max\left(\frac{2\sqrt{k}}{\beta_0^* \omega y}, \frac{500\nu}{y^2 \omega}\right)\right)^2\right]
$$

3. **Production Term.** You can activate a limiter on the production term, P_k , for TMOD =1 and 4. If $C_{\text{cut}} \ge 0$ (CCUT), then:

$$
P_k = \begin{cases} \min(P_k, C_{\text{cut}}\varepsilon) & \text{if TMOD} = 1\\ \min(P_k, C_{\text{cut}}\beta_0^*k\omega) & \text{if TMOD} = 4 \end{cases}
$$

This is especially common when using the Menter SST 2003 model.

- 4. Laws of the Wall for RANS Models. For RANS models, the following laws of the wall are available:
	- a) *Standard Classic (WLAW = 1)*.

$$
U^{+} = \begin{cases} \frac{1}{\kappa} \ln(EY^{+}) & \text{if } Y^{+} > 11.225\\ Y^{+} & \text{otherwise} \end{cases}
$$

$$
Y^{+} = \frac{\rho y U_{\tau}}{\mu}
$$

$$
U^{+} = \frac{U}{U_{\tau}}
$$

$$
U_{\tau} = \sqrt{\frac{\tau_{w}}{\rho}}
$$

This is the default for TMOD = 1.

b) *Standard Launder and Spalding (WLAW = 2).*

$$
U^* = \begin{cases} \frac{1}{\kappa} \ln(EY^*) & \text{if } Y^* > 11.225\\ Y^* & \text{otherwise} \end{cases}
$$

$$
Y^* = \frac{\rho C_{\mu}^{1/4} k^{1/2} y}{\mu}
$$

$$
U^* = \frac{U C_{\mu}^{1/4} k^{1/2}}{U_{\tau}^2}
$$

$$
U_{\tau} = \sqrt{\frac{\tau_w}{\rho}}
$$

c) *Nonequilibrium Launder and Spalding (WLAW = 3).* The nonequilibrium laws of the wall modify the expression of the velocity at the wall making it sensitive to the pressure gradient :

$$
\widetilde{U} = U - \frac{1}{2} \frac{dp}{dx} \left[\frac{y_v}{\rho \kappa \sqrt{k}} ln \left(\frac{y}{y_v} \right) + \frac{y - y_v}{\rho \kappa \sqrt{k}} + \frac{y_v^2}{\mu} \right]
$$

with:

$$
y_v = \frac{11.225}{y^*}y
$$

This law is recommended with $TMOD = 1$ and in cases of complex flows involving separation, reattachment and recirculation.

d) *Automatic Classic (WLAW = 4).* The automatic wall law attempts to blend the viscous and log layers to better account for the transition zone. In the buffer region, we have :

$$
U^{+} = \frac{U}{U_{\tau}}
$$

$$
U_{\tau} = \sqrt[4]{(\frac{U}{y^{+}})^{4} + (\frac{U}{\frac{1}{\pi}\ln(Ey^{+})})^{4}}
$$

This is the recommended approach for TMOD = 4.

5. RANS Turbulence Model with Roughness Included. When a RANS turbulence model is selected, it is possible to define extra parameters to account for roughness effects. In such cases, an extra term will be added to the logarithmic part of the different laws of the wall:

$$
U^+ = \frac{1}{\kappa} \ln(E \, Y^+) - \Delta B
$$

If we introduce the non-dimensional roughness height:

$$
K^+ = \frac{\rho K_s C_\mu^{~1/4} k^{1/2}}{\mu} \ ,
$$

we have:

6. LES Smagorinksy. The LES Smagorinsky turbulence model uses the Van Driest damping function close to the wall:

$$
f_v = 1 - e^{-\frac{y^+}{A^+}}
$$

- 7. LES Dynamic Model. The LES dynamic model is based on the model originally proposed by Germano et. al. (1991) and improved by Lilly (1992), with localization on Cs by Piomelli and Liu (1995).
- 8. Thermal Law of the Wall. When the thermal law of the wall is activated, the turbulent heat flux will be calculated as an additional output variable:

$$
Q_{t} = \rho C_{p} \frac{U_{\tau}}{T_{+}} (T_{s} - T_{c})
$$

\n
$$
T_{+} = \begin{cases} Pr_{t} Y_{+} & \text{if } Y_{+t} \le Y_{+tc} \\ \frac{Pr_{t}}{\vartheta} \log(Y_{+}) + \left(3.85 Pr_{t}^{1.5} - 1.3\right)^{2} + 2.12 \log(Pr_{t}) & \text{otherwise} \end{cases}
$$

*ICFD_CONTROL_TURB_SYNTHESIS

Purpose: This keyword enables the user impose a divergence-free turbulent field on inlets.

Card must be used jointly with $VAD = 4$ of keyword [*ICFD_BOUNDARY_PRE-](#page-362-0)[SCRIBED_VEL.](#page-362-0)

PID Part ID of the surface with the turbulent velocity inlet condition.

IU, IV, IW Intensity of field fluctuations over x , y , and z directions,

$$
IU = \frac{u'}{u_{\text{avg}}}.
$$

LS Integral length scale of turbulence

Remarks:

1. If this card is not defined but a turbulent field inlet has been activated. See VAD = 4 of [*ICFD_BOUNDARY_PRESCRIBED_VEL,](#page-362-0) the default parameters will be used.

*ICFD_DATABASE_AVERAGE

Purpose: This keyword enables the computation of time average variables at given time intervals.

VARIABLE DESCRIPTION

DT Over each DT time interval, an average of the different fluid variables will be calculated and then reset when moving to the next DT interval.

Remarks:

1. The file name for this database is icfdavg.*.dat with the different averaged variable values copied in a ASCII format.

*ICFD_DATABASE_DRAG_{OPTION}

Available options include

VOL

Purpose: This keyword enables the computation of drag forces over given surface parts of the model. If multiple keywords are given, the forces over the PID surfaces are given in separate files and are also added and output in a separate file.

For the VOL option, drag calculation can also be applied on a volume defined by ICFD_PART_VOL. This is mostly useful in porous media applications to output the pressure drag of the porous media domain.

Surface Drag Cards. Include one card for each surface on which drag is applied. This input ends at the next keyword ("*") card.

Remarks:

- 1. The file name for this database is icfdragi for instantaneous drag and icfdraga for the drag computed using average values of pressure and velocities.
- 2. The output contains:
	- a) "Fpx" , "Fpy", and "Fpz" refer to the three components of the pressure drag force

$$
\mathbf{F}_p = \int P dA,
$$

where P is the pressure and A the surface area.

b) "Fvx", "Fxy", and "Fvz" refer to the three components of the viscous drag force

$$
\mathbf{F}_v = \int \mu \frac{\partial \mathbf{u}}{\partial y} \mathrm{d}A.
$$

where $\frac{\partial u}{\partial y}$ is the shear velocity at the wall, μ is the viscosity and A is the surface area.

c) "Mpx", "Mpy", "Mpz", "Mvx", "Mvy", and "Mvz" refer to the three components of the pressure and viscous force moments respectively.

*ICFD_DATABASE_FLUX

Purpose: This keyword enables the computation of the flow rate and average pressure over given parts of the model. If multiple keywords are given, separate files are output.

Include as many cards as needed. This input ends at the next keyword ("*") card.

Remarks:

- 1. Database Name. The file name for this database is icfd_flux.dat.
- 2. Database Components. The flux database contains the flow rate through a section, called "output flux,"

$$
\Phi = \sum_i (\mathbf{V}_i \cdot \mathbf{n}_i) A_i ,
$$

the average pressure, called "Pre-avg,"

$$
P_{\text{avg}} = \frac{\sum_i P_i A_i}{\sum_i A_i} \ ,
$$

and the total area, called "Areatot."

*ICFD_DATABASE_HTC

Purpose: This keyword allows the user to trigger the calculation of the Heat transfer coefficient using different methods and to control the output options.

Remarks:

- 1. The heat transfer coefficient is frequently used in thermal applications to estimate the effect of the fluid cooling and it derived from a CFD calculation.
- 2. The heat transfer coefficient is defined as follows:

$$
h = \frac{q}{T_s - T_b}
$$

with q the heat flux, T_s the surface temperature and T_b the so called "bulk" temperature. For external aerodynamic applications, this bulk temperature is often defined as a constant (ambient or far field conditions, HTC = 1). However, for internal aerodynamic application, this temperature is often defined as an average temperature flowing through the pipe section with the flow velocity being used as a weighting factor ($HTC = 0$).

*ICFD_DATABASE_**NODEAVG**

Purpose: This keyword enables the computation of the average quantities on surface nodes defined in *ICFD_DATABASE_NODOUT.

VARIABLE DESCRIPTION

ON If equal to 1, the average quantities will be computed.

Remarks:

1. The file name for this database is icfd_nodeavg.dat.

*ICFD_DATABASE_**NODOUT**

Purpose: This keyword enables the output of ICFD data on surface nodes. For data in the fluid volume, it is advised to use points or tracers (See *ICFD_DATABASE_- POINTOUT).

Output Options Card.

Include as many cards as needed. This input ends at the next keyword ("*") card.

DESCRIPTION

NID.. Node IDs.

Remarks:

1. The file name for this database is icfd_nodout.dat.

*ICFD_DATABASE_**POINTAVG**

Purpose: This keyword enables the computation of the average quantities on point sets using the parameters defined in *ICFD_DATABASE_POINTOUT.

VARIABLE DESCRIPTION

ON If equal to 1, the average quantities will be computed.

Remarks:

1. The file name for this database is icfd_psavg.dat.

*ICFD_DATABASE_**POINTOUT**

Purpose: This keyword enables the output of ICFD data on points.

Output Options Card.

Include as many cards as needed. This input ends at the next keyword ("*") card.

X, Y, Z Point initial coordinates

Remarks:

1. The file name for this database is icfd_pointout.dat.

*ICFD_DATABASE_RESIDUALS

Purpose: This keyword allows the user to output the residuals of the various systems.

VARIABLE DESCRIPTION

RLVL Residual output level :

EQ.0: No output.

- EQ.1: Only outputs the number of iterations needed for solving the pressure Poisson equation.
- EQ.2: Outputs the number of iterations for the momentum, pressure, mesh movement and temperature equations.
- EQ.3: Also gives the residual for each iteration during the solve of the momentum, pressure, mesh movement and temperature equations.

Remarks:

1. The file names for the momentum, pressure, mesh movement and temperature equations are called icfd_residuals.moms.dat, icfd_residuals.pres.dat, icfd_ residuals.mmov.dat, and icfd_residuals.temp.dat respectively.

*ICFD_DATABASE_**TEMP**

Purpose: This keyword enables the computation of the average temperature and the heat flux over given parts of the model. If multiple keywords are given, separate files are output.

Include as many cards as needed. This input ends at the next keyword ("*") card.

VARIABLE DESCRIPTION

Remarks:

- 1. The file name for this database is icfd_thermal.dat.
- 2. Two average temperature are given in the icfd_thermal.dat file: "Temp-avg" and "Temp-sum". The average temperature is calculated using the local node area as weighting factor,

$$
T_{\text{avg}} = \frac{\sum_{i}^{N} T_{i} A_{i}}{\sum_{i}^{N} A_{i}},
$$

whereas, the sum is not weighted by area

$$
T_{\text{sum}} = \frac{\sum_{i}^{N} T_{i}}{N}
$$

If the mesh is regular, the two values will be of similar value. The icfd_thermal.dat output file also includes the average heat flux, the total surface area, and the average heat transfer coefficients (See *ICFD_DATABASE_HTC).

*ICFD_DATABASE_**TIMESTEP**

Purpose: This keyword enables the output of ICFD data regarding the ICFD timestep.

Output Options Card.

VARIABLE DESCRIPTION

OUTLV Determines if the output file should be dumped.

EQ.0: No output file is generated.

EQ.1: The output file is generated.

Remarks:

- 1. The file name for this database is icfd_tsout.dat.
- 2. Outputs the run's ICFD timestep versus the timestep calculated using the ICFD CFL condition as criteria (autotimestep). This can be useful in cases using a fixed timestep where big mesh deformations and/or big fluid velocity changes occur in order to track how that fixed timestep value compares to the reference autotimestep.

*ICFD_DATABASE_UINDEX

Purpose: This keyword allows the user to have the solver calculate the uniformity index (See [Remark 1\)](#page-424-0).

VARIABLE DESCRIPTION

OUT Determines if the solver should calculate the uniformity index. EQ.0: Off. EQ.1: On.

Remarks:

1. **Uniformity Index.** The uniformity index is a post treatment quantity which measures how uniform the flow is through a given section. It is especially useful in internal aerodynamics cases. It is expressed as :

$$
\gamma = 1 - \frac{1}{2nA} \sum_{i=1}^{n} \left[\frac{\sqrt{(u_i - \bar{u})^2}}{\bar{u}} A_i \right]
$$

with A_i , the local cell area, A the total section area, u_i the local velocity, \bar{u} the average velocity through the section, and n the number of cells.

Values close to 0 means that the flow is very unevenly distributed. This can be used to identify bends, corners or turbulent effects. Values close to 1 imply smooth or equally distributed flow through the surface.

*ICFD_DEFINE_**HEATSOURCE**

Purpose: This keyword defines a volumetric heat source for the heat equation solve.

.

*ICFD_DEFINE_SOURCE

Purpose: Define a volumetric external force for the momentum equation solve.

*ICFD_DEFINE_**TURBSOURCE**

Purpose: This keyword defines a external source for the RANS turbulent equations.

.

*ICFD_DEFINE_POINT

Purpose: This keyword defines a point in space that could be used for multiple purposes.

Optional Card 2. Load curve IDS specifying velocity components of translating point

Optional Card 3. Load curve IDS and rotation axis of rotating point

VARIABLE DESCRIPTION

POID Point ID.

 $X/Y/Z$ x, y ,z coordinates for the point.

.

*ICFD_DEFINE_NONINERTIAL

Purpose: This keyword defines a non-inertial reference frame in order to avoid heavy mesh distortions and attendant remeshing associated with large-scale rotations. This is used to model, for example, spinning cylinders, wind turbines, and turbo machinery.

Include as many cards as needed. This input ends at the next keyword ("*") card.

DESCRIPTION

- W1, W2, W3 Rotational Velocity along the X,Y,Z axes
	- R Radius of the rotating reference frame. If a negative value if given, then the absolute value will refer to a *DEFINE_FUNC-TION ID. If a DEFINE_FUNCTION is used, the following parameters are allowed: $f(x, y, z, vx, vy, vz, temp, pres, time)$.
	- PTID Starting point ID for the reference frame (See *ICFD_DEFINE_- POINT)
		- L Length of the rotating reference frame

Figure 7-2. Non Inertial Reference Frame Example

*ICFD_DEFINE_WAVE_DAMPING

Purpose: This keyword defines a damping zone for free surface waves.

1. The damping is achieved by adding a source term to the momentum equations :

$$
s^d = w \left(f_1 + f_2 |u| \right) u
$$

with w the weight function :

$$
w = \frac{e^{\gamma} - 1}{e - 1}
$$

and γ the blending function which allows a smooth insertion of the source term in the damping layer :

$$
\gamma = \left(\frac{x - x_{sd}}{x_{ed} - x_{sd}}\right)^n
$$

 x_{sd} and x_{ed} representing the start and end coordinates of the damping zone.

*ICFD_INITIAL

Purpose: Simple initialization of velocity and temperature within a volume.

Include as many cards as needed. This input ends at the next keyword ("*") card.

*ICFD_INITIAL_LEVELSET

Purpose: Instead of defining multiple fluid domain, it is possible to define an initial levelset surface via the introduction of this keyword (Replaces the need for *MESH_IN-TERF keyword).

Include as many cards as needed. This input ends at the next keyword ("*") card.

Remarks:

1. When $STYPE = 2$ is used and the box is adjacent to the fluid boundaries such as in dam breaking cases, it is important to define the Pmin coordinates far outside the domain so that, at any point in the fluid, the distance to the fluid boundary remains smaller than the distance to the defined box.

Figure [1]. 2D Dam breaking example with initial levelset surface defined using STYPE = 2. Pmin is defined sufficiently far away from the fluid surface boundaries.

*ICFD_INITIAL_TURBULENCE

Purpose: When a RANS turbulent model is selected, it is possible to modify the default initial values of the turbulent quantities using this keyword.

VARIABLE DESCRIPTION

Remarks:

1. If no initial conditions have been assigned to a specific PID, the solver will automatically pick I = 0.05 (5%) and R = 10000.

*ICFD_MAT_{OPTION}

Available options include

TITLE

Purpose: Specify physical properties for the fluid material.

Fluid Material Card Sets:

The Material Fluid Parameters Card is required. If a second card is given, it must be a Thermal Fluid Parameters Card. If the fluid thermal properties are not needed, the second card can be a blank card. With the third card, you can associate the fluid material to a non-Newtonian model and/or to a porous media model (see *ICFD_MOD-EL_NONNEWT and *ICFD_MODEL_POROUS).

Material Fluid Parameters Card.

Thermal Fluid Parameters Card. Only to be defined if the thermal problem is solved.

Additional fluid models. Only to be defined if the fluid is non-Newtonian and/or is a porous media.

VARIABLE DESCRIPTION

FINE_FUNCTION. If a *DEFINE_FUNCTION is used, the following parameters are allowed: f(x, y, z, vx, vy, vz, temp, pres, time).

- TCSFLCID Load curve ID for scale factor applied on TC function of time. See *DEFINE_CURVE, *DEFINE_CURVE_FUNCTION, or *DE-FINE_FUNCTION. If a *DEFINE_FUNCTION is used, the following parameters are allowed: f(x, y, z, vx, vy, vz, temp, pres, time).
- NNMOID Non-Newtonian model ID. This refers to a Non-Newtonian fluid model defined using *ICFD_MODEL_NONNEWT.
- PMMOID Porous media model ID. This refers to a porous media model defined using *ICFD_MODEL_POROUS.

*ICFD_MODEL_NONNEWT

Purpose: Specify a non-newtonian model or a viscosity law that can associated to a fluid material.

Non-Newtonian Model ID and type.

Non-Newtonian Fluid Parameters Card.

VARIABLE DESCRIPTION

NNMOID Non-Newtonian Model ID.

NNID Non-Newtonian fluid model type :

EQ.1 : Power-Law model

EQ.2 : Carreau model

EQ.3 : Cross model

EQ.4 : Herschel-Bulkley model

EQ.5 : Cross II model

EQ.6 : Sutherland formula for temperature dependent viscosity

EQ.7 : Power-Law for temperature dependent viscosity

EQ.8 : Viscosity defined by Load Curve ID or Function ID

VARIABLE DESCRIPTION

Remarks:

- 1. For the Non-Newtonian models, the viscosity is expressed as :
	- a) POWER-LAW :

$$
\mu = k\dot{\gamma}^{n-1} e^{\alpha T_0/T}
$$

$$
\mu_{min} < \mu < \mu_{max}
$$

With k the consistency index, n the power law index, α the activation energy, T_0 the initial temperature, T the temperature at any given time t , μ_{min} the minimum acceptable viscosity and μ_{max} the maximum acceptable viscosity.

b) CARREAU :

$$
\mu = \mu_{\infty} + (\mu_0 - \mu_{\infty}) \left[1 + (H(T)\dot{\gamma}\lambda)^2 \right]^{(n-1)/2}
$$

$$
H(T) = \exp\left[\alpha \left(\frac{1}{T - T_0} - \frac{1}{T_{\alpha} - T_0} \right) \right]
$$

With μ_{∞} the infinite shear viscosity, μ_0 the zero shear viscosity, *n* the power law index, λ a time constant, α the activation energy, T_0 the initial temperature, T

the temperature at any given time t and T_{α} the reference temperature at which $H(T) = 1.$

c) CROSS :

$$
\mu = \frac{\mu_0}{1 + (\lambda \dot{\gamma})^{1-n}}
$$

With μ_0 the zero shear viscosity, *n* the power law index and λ a time constant.

d) HERSCHEL-BULKLEY :

$$
\mu = \mu_0 \text{ if } (\dot{\gamma} < \tau_0 / \mu_0)
$$
\n
$$
\mu = \frac{\tau_0 + k[\dot{\gamma}^n - (\tau_0 / \mu_0)^n]}{\dot{\gamma}}
$$

With *k* the consistency index, τ_0 the Yield stress threshold, μ_0 the yielding viscosity and n the power law index.

e) CROSS II :

$$
\mu = \mu_\infty + \frac{\mu_0 - \mu_\infty}{1 + (\lambda \dot{\gamma})^n}
$$

With μ_0 the zero shear viscosity, μ_{∞} the infinite shear viscosity, *n* the power law index and λ a time constant.

- 2. For the temperature dependent viscosity models, the viscosity is expressed as :
	- a) SUTHERLAND's LAW :

$$
\mu = \mu_0 \left(\frac{T}{T_0}\right)^{3/2} \frac{T_0 + S}{T + S}
$$

With μ_0 a reference viscosity, T_0 the initial temperature (which therefore must not be 0 .), T the temperature at any given time t and S Sutherland's constant.

b) POWER LAW :

$$
\mu=\mu_0(\frac{T}{T_0})^n
$$

With μ_0 a reference viscosity, T_0 the initial temperature (which therefore must not be 0.), T the temperature at any given time t and n the power law index.

3. For NNID = 8 , a load curve function of time, a curve function or a function can be used. If it references a DEFINE_FUNCTION, the following arguments are allowed $f(x, y, z, vx, vy, vz, temp, pres, shear, time)$.

*ICFD_MODEL_POROUS

Purpose: Specify a porous media model.

Card Summary:

[Card 2a.](#page-448-0) This card is included if $PMMTYPE = 1, 2,$ or 8.

[Card 2b.](#page-448-1) This card is included if PMMTYPE = 3 or 10.

[Card 2c.](#page-449-0) This card is included if $\text{PMMTYPE} = 4, 6, \text{ or } 7$.

[Card 2d.](#page-449-1) This card is included if $PMMTYPE = 5$.

[Card 2e.](#page-450-0) This card is included if $PMMType = 11$.

[Card 3.](#page-450-1) This card is included if $\text{PMMTYPE} = 4, 5, 6, \text{ or } 7$

[Card 4a.](#page-451-0) This card is included if PMMTYPE = 4 or 6.

[Card 4b.](#page-451-1) This card is included if $PMMTYPE = 5$ or 7.

Data Card Definitions:

VARIABLE DESCRIPTION

EQ.11: Parachute model similar to $PMMType = 8$, but pressure gradient is directly defined by coefficients α and β as:

$$
\frac{\Delta P(u_x)}{\Delta x} = \alpha u_x + \beta u_x^2.
$$

Porous Media Parameters Card (PMMTYPE = 1, 2, and 8). This card is included $PMMTYPE = 1, 2,$ or 8.

VARIABLE DESCRIPTION

POR Porosity, ε

PER Permeability, κ

FF Forchheimer factor to be defined if PMMTYPE $= 2$ or 8.

PSFLCID Optional permeability scale factor load curve ID, *DEFINE_- CURVE_FUNCTION ID or *DEFINE_FUNCTION ID for PMM- $TYPE = 1$ or 2. If a *DEFINE_FUNCTION is used, the following parameters are allowed: f(x, y, z, vx, vy, vz, temp, pres, time).

Porous Media Parameters Card (PMMTYPE = 3 and 10). This card is included if $PMMTYPE = 3$ or 10.

Porous Media Parameters Card (PMMTYPE = 4, 6, and 7). This card is included if $PMMTYPE = 4, 6, or 7.$

VARIABLE DESCRIPTION

POR Porosity, ε

Porous Media Parameters Card (PMMTYPE = 5). This card is included if PMM- $TYPE = 5.$

- POR Porosity, ε
- THX Probe thickness, Δx
- THY Probe thickness, Δy

*ICFD_MODEL_POROUS *ICFD

Porous Media Parameters Card (PMMTYPE = 11). This card is included if PMM- $TYPE = 11.$

VARIABLE DESCRIPTION

POR Porosity, ε

ALPHA Coefficient, α

BETA Coefficient, β

Permeability Vector Card in local reference frame. Only to be defined if the porous media is anisotropic (PMMTYPE = 4, 5, 6, 7).

VARIABLE DESCRIPTION

KXP, KYP, KZP Permeability vector in local reference frame (x', y', z') . Those values become scale factors if PMMTYPE = 5.

Projection of Local Vectors in Global Reference Frame. This card is defined if $PMMTYPE = 4$ or 6.

VARIABLE DESCRIPTION

Local Reference Frame Vectors. This card is defined if PMMTYPE = 5 or 7.

VARIABLE DESCRIPTION

PID1REF, PID2REF Two local reference frame vectors are defined by the coordinates of the two-point IDs defined by PID1REF and PID2REF. (See

Figure 7-3. Anisotropic porous media vectors definition (PMMTYPE = 4 , 5 , 6 , and 7). The vectors **X** and **Y** are the global axes; **x'** and **y'** define system for the primed coordinate (x', y', z') .

VARIABLE DESCRIPTION

*ICFD_DEFINE_POINT). Since those points can be made to move, it is therefore possible to define a moving reference frame for the anisotropic porous media domain.

Remarks:

1. Generalized Flow Equations in a Porous Media. Let ε be the porosity and κ be the permeability of the porous media. Then,

$$
\varepsilon = \frac{\text{void volume}}{\text{total volume}}.
$$

 u_i , the volume averaged velocity field, can then be defined in terms of the fluid velocity field, u_{if} , as:

$$
u_i = \varepsilon u_{if} .
$$

The generalized flow equations of momentum and mass conservation can be expressed as:

$$
\frac{\partial u_i}{\partial x_i} = 0
$$

$$
\frac{\rho}{\varepsilon} \left[\frac{\partial u_i}{\partial t} + \frac{\partial}{\partial x_j} \frac{\partial u_i u_j}{\varepsilon} \right] = -\frac{1}{\varepsilon} \frac{\partial (P\varepsilon)}{\partial x_i} + \frac{\mu}{\varepsilon} \left(\frac{\partial^2 u_i}{\partial x_j \partial x_j} \right) + \rho g_i - D_i
$$

where D_i are the forces exerted on the fluid by the porous matrix (see [Re](#page-453-0)[marks 2](#page-453-0) and [3\)](#page-453-1).

- 2. Porous Forces for Isotropic Models. For the isotropic model, the porous forces are a function of the matrix porosity and its permeability. For the isotropic case, three models are available:
	- a) *Model 1 (Ergun correlation).*

$$
D_i = \frac{\mu u_i}{\kappa} + \frac{1.75\rho|U|}{\sqrt{150}\sqrt{\kappa}\varepsilon^{3/2}}u_i
$$

b) *Model 2 (Darcy-Forcheimer).*

$$
D_i = \frac{\mu u_i}{\kappa} + \frac{F \varepsilon \rho |U|}{\sqrt{\kappa}} u_i
$$

- c) *Model 3.* Using the $\Delta P V$ experimental data. In this case, it is assumed that the pressure-velocity curve was obtained by applying a pressure difference or pressure drop on both ends of a porous slab of thickness Δx with porous properties κ and ε . It then becomes possible for the solver to fit that experimental curve with a quadratic polynomial of the form $\Delta P(u_x) = \alpha {u_x}^2 + \beta u_x$. Once α and β are known, it is possible to estimate D_i .
- 3. **Anisotropic Darcy-Forcheimer Term.** The anisotropic (see Figure 0-1) version of the Darcy-Forcheimer term can be written as:

$$
D_i = \mu B_{ij} \mu_j + F \varepsilon |U| C_{ij} u_j
$$

\n
$$
B_{ij} = (K_{ij})^{-1}
$$

\n
$$
C_{ij} = (K_{ij})^{-1/2}
$$

Here K_{ii} is the anisotropic permeability tensor.

*ICFD_PART_{OPTION}

Available options include

TITLE

Purpose: Define parts for this incompressible flow solver.

The TITLE option allows the user to define an additional optional line with a HEADING in order to associate a name to the part.

Part Material Card. Include as many cards as needed. This input ends at the next keyword ("*") card.

*ICFD_PART_VOL_{OPTION}

Available options include

TITLE

Purpose: This keyword assigns material properties to the nodes enclosed by surface ICFD parts.

The TITLE option allows the user to define an additional optional line with a HEAD-ING in order to associate a name to the part.

Provide as many cards as necessary. This input ends at the next keyword ("*") card

*ICFD_PART_VOL *ICFD

SPID1, ... Part IDs for the surface elements that define the volume mesh.

PID 3

```
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$ 
$$$$ *ICFD_PART_VOL
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$ 
$ 
$ PART ID 5 is defined by the surfaces that enclose it. 
\ddot{\varsigma}*ICFD_PART_VOL 
\ddot{\varsigma}$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8 
\begin{tabular}{llllll} $\mathfrak{s}$ & $\mathfrak{pid}$ & $\mathfrak{secid}$ & $\mathfrak{mid}$ \\ & $\mathfrak{b}$ & $\mathfrak{1}$ & $\mathfrak{1}$ \\ \end{tabular} 5 1 1 
$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8 
$ pid1 pid2 pid3 pid4 pid5 pid6 pid7 pid8 
 1 2 3 4
```
PID 3

*ICFD_SECTION

Purpose: Define a section for the incompressible flow solver.

VARIABLE DESCRIPTION

SID Section identifier.

*ICFD_SET_NODE_LIST

Purpose: Only used in cases where the mesh is specified by the user (See *MESH_VOLUME_ELEMENT). Defines a set of nodes associated with a part ID on which boundary conditions can be applied.

Node List Card. Provide as many cards as necessary. This input ends at the next keyword ("*") card

VARIABLE DESCRIPTION

- SID Set ID
- PID Associated Part ID.

NID1, … Node IDs

Remarks:

1. The convention is the similar to the one used by the keyword *SET_NODE_LIST and serves a similar purpose.

*ICFD_**SOLVER**_SPLIT

Purpose: This keyword provides an option to trigger an iterative procedure on the fluid system. This procedure aims to bring more precision to the final pressure and velocity values but is often very time consuming. It must therefore be used with caution. It is intended only for special cases. For stability purposes, this method is automatically used for the first ICFD time step.

TOL Tolerance Criteria for the pressure residual during the fluid system solve.

*ICFD_SOLVER_TOL_FSI

Purpose: This keyword allows the user to change the default tolerance values for the Newton Raphson loop in the strong FSI analysis. *Care should be taken when deviating from the default values*.

- ATOL Absolute convergence criteria. Convergence is achieved when Residual_{*i*+1} – Residual_{*i*} \leq ATOL. If a negative integer is entered, then that value will be used as a load curve ID for ATOL.
- RTOL Relative convergence criteria. Convergence is achieved when (Residual_{*i*+1} – Residual_{*i*})/Residual_{initial} \leq *RTOL*. If a negative integer is entered, then that value will be used as a load curve ID for RTOL.
- MAXIT Maximum number of iterations allowed to achieve convergence. If a negative integer is entered, then that value will be used as a load curve ID for MAXIT.

*ICFD_SOLVER_TOL_LSET

Purpose: This keyword allows the user to change the default tolerance values for the advection equation for levelset. *Care should be taken when deviating from the default values*.

- ATOL Absolute convergence criteria. Convergence is achieved when Residual_{*i*+1} – Residual_{*i*} \leq ATOL. If a negative integer is entered, then that value will be used as a load curve ID for ATOL.
- RTOL Relative convergence criteria. Convergence is achieved when (Residual_{*i*+1} – Residual_{*i*})/Residual_{initial} \leq *RTOL*. If a negative integer is entered, then that value will be used as a load curve ID for RTOL.
- MAXIT Maximum number of iterations allowed to achieve convergence. If a negative integer is entered, then that value will be used as a load curve ID for MAXIT.

*ICFD_SOLVER_TOL_MMOV

Purpose: This keyword allows the user to change the default tolerance values for the mesh movement algorithm. *Care should be taken when deviating from the default values*.

- ATOL Absolute convergence criteria. Convergence is achieved when Residual_{$i+1$} – Residual_i \leq ATOL. If a negative integer is entered, then that value will be used as a load curve ID for ATOL.
- RTOL Relative convergence criteria. Convergence is achieved when (Residual_{*i*+1} – Residual_{*i*})/Residual_{initial} \leq RTOL. If a negative integer is entered, then that value will be used as a load curve ID for RTOL.
- MAXIT Maximum number of iterations allowed to achieve convergence. If a negative integer is entered, then that value will be used as a load curve ID for MAXIT.
- DISPTOL Element deformation tolerance before a matrix reassembly is triggered. Default is 0. which means any element deformation detected will automatically trigger a matrix reassembly. Higher values will potentially save calculation times at the expense of accuracy.

*ICFD_**SOLVER_TOL_MOM**

Purpose: This keyword allows the user to change the default tolerance values for the momentum equation solve. *Care should be taken when deviating from the default values*.

- ATOL Absolute convergence criteria. Convergence is achieved when Residual_{*i*+1} – Residual_{*i*} \leq ATOL. If a negative integer is entered, then that value will be used as a load curve ID for ATOL.
- RTOL Relative convergence criteria. Convergence is achieved when $(Residual_{i+1} - Residual_i)/Residual_{initial} \leq RTOL$. If a negative integer is entered, then that value will be used as a load curve ID for RTOL.
- MAXIT Maximum number of iterations allowed to achieve convergence. If a negative integer is entered, then that value will be used as a load curve ID for MAXIT.

*ICFD_**SOLVER_TOL_MONOLITHIC**

Purpose: This keyword allows the user to change the default tolerance values for the monolithic solver. *Care should be taken when deviating from the default values*.

- ATOL Absolute convergence criteria. Convergence is achieved when Residual_{*i*+1} – Residual_{*i*} \leq ATOL. If a negative integer is entered, then that value will be used as a load curve ID for ATOL.
- RTOL Relative convergence criteria. Convergence is achieved when $(Residual_{i+1} - Residual_i)/Residual_{initial} \leq RTOL$. If a negative integer is entered, then that value will be used as a load curve ID for RTOL.
- MAXIT Maximum number of iterations allowed to achieve convergence. If a negative integer is entered, then that value will be used as a load curve ID for MAXIT.

*ICFD_SOLVER_TOL_PRE

Purpose: This keyword allows the user to change the default tolerance values for the Poisson equation for pressure. *Care should be taken when deviating from the default values*.

- ATOL Absolute convergence criteria. Convergence is achieved when Residual_{*i*+1} – Residual_{*i*} \leq ATOL. If a negative integer is entered, then that value will be used as a load curve ID for ATOL.
- RTOL Relative convergence criteria. Convergence is achieved when (Residual_{*i*+1} – Residual_{*i*})/Residual_{initial} \leq *RTOL*. If a negative integer is entered, then that value will be used as a load curve ID for RTOL.
- MAXIT Maximum number of iterations allowed to achieve convergence. If a negative integer is entered, then that value will be used as a load curve ID for MAXIT.

*ICFD_SOLVER_TOL_TEMP

Purpose: This keyword allows the user to change the default tolerance values for the heat equation. To be handled with great care.

- ATOL Absolute convergence criteria. Convergence is achieved when $Residual_{i+1}$ – $Residual_i \leq ATOL$. If a negative integer is entered, then that value will be used as a load curve ID for ATOL.
- RTOL Relative convergence criteria. Convergence is achieved when $(Residual_{i+1} - Residual_i) / Residual_{initial} \le RTOL$. If a negative integer is entered, then that value will be used as a load curve ID for RTOL.
- MAXIT Maximum number of iterations allowed to achieve convergence. If a negative integer is entered, then that value will be used as a load curve ID for MAXIT.
*MESH

The keyword *MESH is used to create a mesh that will be used in the analysis. So far only tetrahedral (or triangular in 2-d) elements can be generated. The keyword cards in this section are defined in alphabetical order:

*MESH_BL

*MESH_BL_SYM

*MESH_EMBEDSHELL

*MESH_INTERF

*MESH_NODE

*MESH_SIZE_

*MESH_SIZE_SHAPE

*MESH_SURFACE_ELEMENT

*MESH_SURFACE_NODE

*MESH_VOLUME

*MESH_VOLUME_ELEMENT

*MESH_VOLUME_NODE

*MESH_VOLUME_PART

*MESH *MESH_BL

*MESH_BL

Purpose: This keyword is used to define a boundary-layer mesh as a refinement on volume-mesh. The boundary layer mesh is constructed by subdividing elements near the surface.

Boundary Layer Cards. Define as many cards as are necessary. The next "*" card terminates the input.

EQ.3: Repartition following a growth scale factor (BLTH).

Remarks:

- 1. For $BLST = 0$, for every additional NELTH, the automatic volume mesher will divide the elements closest to the surface by two so that the smallest element in the boundary layer mesh will have an aspect ratio of $2^{NELTH+1}$. A default boundary layer mesh thickness based on the surface mesh size will be chosen.
- 2. For a constant repartition of the nodes in the boundary layer, use $B LST = 1$ with BLFE = 1. For BLST = 1, starting from the wall, the position of node n in the normal direction is given by :

Figure [1]. $BLST = 1$ example

3. Setting BLFE = 1 makes BLST = 2 equivalent to BLST = 0 except that BLST = 0 allows BLTH to be specified by the user instead of automatically using the local surface mesh size. For BLST = 2, starting from BLTH, each newly inserted node will have its location closer to the wall, following this law :

$$
X_n = (0.5 \times BLTE)^n * BLTH * (1 - 0.5 * BLTE)
$$

Figure [2]. $BLST = 2$ example

4. For $BLST = 3$, starting from the wall, the position of node n in the normal direction is given by :

$$
X_n = \sum_{i=0}^{n} BLE \times BLTH^i \text{ with } 0 \le n \le NELTH
$$

Figure [3]. $BLST = 3$ example

*MESH_BL_SYM

Purpose: Specify the part IDs that will have symmetry conditions for the boundary layer. On these surfaces, the boundary layer mesh follows the surface tangent.

Boundary Layer with Symmetry Condition Cards. Define as many cards as necessary. The next "*" card terminates the input.

VARIABLE DESCRIPTION

PID1, ... Part identifiers for the surface element. This is the surface with symmetry.

*MESH_EMBEDSHELL

Purpose: Define surfaces that the mesher will embed inside the volume mesh. These surfaces will have no thickness and will conform to the rest of the volume mesh having matching nodes on the interface.

Define as many cards as are necessary based on the number of PIDs (the next "*" card terminates the input.)

VARIABLE DESCRIPTION

- VOLID ID assigned to the new volume in the keyword *MESH_VOL-UME. The surface mesh size will be applied to this volume.
- PID*n* Part IDs for the surface elements that will be embedded in the volume mesh.

*MESH_INTERF

Purpose: Define the surfaces that will be used by the mesher to specify fluid interfaces in multi-fluid simulations.

Define as many cards as are necessary based on the number of PIDs. This input ends at the next keyword ("*") card.

VARIABLE DESCRIPTION

VOLID ID assigned to the new volume in the keyword *MESH_VOL-UME. The interface meshes will be applied to this volume.

PID*n* Part IDs for the surface elements.

*MESH_NODE

Purpose: Define a fluid node and its coordinates. These nodes are used in the mesh generation process by the *MESH_SURFACE_ELEMENT keyword, or as user defined volume nodes by the *MESH_VOLUME_ELEMENT keyword.

Node Cards. Include one additional card for each node. This input ends at the next keyword ("*") card.

VARIABLE DESCRIPTION

NID Node ID. A unique number with respect to the other surface nodes. $X \sim x$ coordinate. Y coordinate. Z *z* coordinate.

Remarks:

- 1. The data card format for the *MESH_NODE keyword is identical to *NODE.
- 2. The *MESH_NODE keyword supersedes *MESH_SURFACE_NODE, which was for surfaces nodes as well as *MESH_VOLUME_NODE for, which was for volume nodes in user defined.

*MESH_SIZE

Purpose: Define the surfaces that will be used by the mesher to specify a local mesh size inside the volume. If no internal mesh is used to specify the size, the mesher will use a linear interpolation of the surface sizes that define the volume enclosure**.**

Define as many cards as are necessary based on the number of PIDs (the next "*" card terminates the input.).

VARIABLE DESCRIPTION

- VOLID ID assigned to the new volume in the keyword *MESH_VOL-UME. The mesh sizing will be applied to this volume.
- $PIDn$ Part IDs for the surface elements that are used to define the mesh size next to the surface mesh.

*MESH_SIZE_SHAPE

Purpose: Defines a local mesh size in specific zones corresponding to given geometrical shapes (box, sphere, cylinder and polynomial). The solver will automatically apply the conditions specified during the generation of the volume mesh. This zone does not need to be entirely defined in the volume mesh. In the polynomial case, it is recommended to define several zones for a better mesh size control.

Remeshing Control Card sets:

Add as many *remeshing control cards* paired with a *case card* as desired. The input of such pairs ends at the next keyword "*" card.

Remeshing Control. First card specifies whether to maintain this mesh sizing criterion through a remesh operation.

Card 1		$\overline{2}$	3	4	5	6	8
Variable	SNAME	FORCE	METHOD	BT	DT		
Type	A			F	F		
Default	none	$\mathbf 0$	0	0.	1.E12		

Box Case. Card 2 for $SNAME = "box"$ and $METHOD = 0$

Sphere Case. Card 2 for $SNAME = "sphere"$ and $METHOD = 0$

Cylinder Case. Card 2 for $SNAME = "cylinder"$ and $METHOD = 0$

Polynomial Case. Card 2 for $SNAME = "pol"$ and $METHOD = 0$

Card 2 for $METHOD = 1$

Cards 2		$\overline{2}$	3	4	5	6	8
Variable	MSIZE	RADIUS	PTID1	PTID ₂			
Type	F	F					
Default	none	none	none	none			

*MESH_SURFACE_ELEMENT

Purpose: Specify a set of surface elements (quadrilateral or triangular in 3-d and linear segments in 2-d) that will be used by the mesher to construct a volume mesh. These surface elements may be used to define the enclosed volume to be meshed, or alternatively they could be used to apply different mesh sizes inside the volume (see card *MESH_SIZE**).**

Surface Element Card. Define as many cards as necessary. The next "*" card terminates the input.

VARIABLE DESCRIPTION

Remarks:

1. The convention is the same used by the keyword *ELEMENT_SHELL. In the case of a triangular face $N3 = N4$. In $2-d$ $N2 = N3 = N4$. Note that the accepted card format is 6i8 (not 6i10)

*MESH_SURFACE_NODE

Purpose: Define a node and its coordinates. These nodes will be used in the mesh generation process by the *MESH_SURFACE_ELEMENT keyword.

*MESH_NODE supersedes this card; so please use *MESH_NODE instead of this card.

Surface Node Cards. Include one card for each node. Include as many cards a necessary. This input ends at the next keyword ("*") card.

VARIABLE DESCRIPTION

Z z coordinate.

*MESH_VOLUME

Purpose: This keyword defines the volume space that will be meshed. The boundaries of the volume are the surfaces defined by *MESH_SURFACE_ELEMENT. The surfaces listed have to be non-overlapping, and should not leave any gaps or open spaces between the surface boundaries. On the boundary between two neighbor surfaces, nodes have to be in common (no duplicate nodes) and should match exactly on the interface. They are defined by the keyword *MESH_SURFACE_NODE. This card will be ignored if the volume mesh is specified by the user and not generated automatically.

Define as many cards as are necessary based on the number of PIDs (the next "*" card terminates the input.)

VARIABLE DESCRIPTION

VOLID **ID** assigned to the new volume.

PID*n* Part IDs for the surface elements that are used to define the volume.

*MESH_VOLUME_ELEMENT

Purpose: Specify a set of volume elements for the fluid volume mesh in cases where the volume mesh is specified by the user and not generated automatically. The nodal point are specified in the *MESH_VOLUME_NODE keyword. Only tetrahedral elements are supported (triangles in 2D).

Volume Element Card. Define as many cards as necessary. The next "*" card terminates the input.

VARIABLE DESCRIPTION

Remarks:

1. The convention is the same used by the keyword *ELEMENT_SOLID.

*MESH_VOLUME_NODE

Purpose: Define a node and its coordinates. This keyword is only used in cases where the fluid volume mesh is provided by the user and is not automatically generated. It serves the same purpose as the *NODE keyword for solid mechanics. Only tetrahedral elements are supported**.**

*MESH_NODE supersedes this card; so please use *MESH_NODE instead of this card.

Volume Node Cards. Include as many cards in the following format as desired. This input ends at the next keyword ("*") card.

VARIABLE DESCRIPTION

*MESH_VOLUME_PART

Purpose: Associate a volume part number created by a *MESH_VOLUME card with the part number of a part card from a selected solver (designated by the SOLVER field).

Mesh Volume Part Card. Include as many cards in the following format as desired. This input ends at the next keyword ("*") card.

*STOCHASTIC

The keyword *STOCHASTIC is used to describe the particles and numerical details for solving a set of stochastic PDEs. Currently, there are two types of stochastic PDE models in the code: a spray model and a model of embedded particles in TBX explosives. The keyword cards for using these models are:

*STOCHASTIC_SPRAY_PARTICLES

*STOCHASTIC_TBX_PARTICLES

An additional option "**_**TITLE**"** may be appended to all *STOCHASTIC keywords. If this option is used, then an 80 character string is read as a title from the first card of that keyword's input. At present, LS-DYNA does not make use of the title. Inclusion of titles gives greater clarity to input decks.

*STOCHASTIC_SPRAY_PARTICLES

Purpose: Specify particle and other model details for spray modeling using stochastic PDEs that approximate such processes. A pair of cards is required to specify the characteristics of each nozzle (cards 3 and 4 describe the first nozzle).

Nozzle card 1: Provide as many pairs of nozzle cards 1 and 2 as necessary. This input ends at the next keyword ("*") card (following a nozzle card 2).

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Nozzle card 2: Provide as many pairs of nozzle cards 1 and 2 as necessary. This input ends at the next keyword ("*") card.

Remarks:

1. When IEVAP = 1, the keyword input file must be modified in a fashion similar to a chemistry problem. This is illustrated in a portion of an example keyword file below. That is, the following keywords need to be used, along with the inclusion of other chemistry-related files (i.e. evap.inp and the corresponding thermodynamics data file):

*CHEMISTRY_MODEL *CHEMISTRY_COMPOSITION *CHEMISTRY_CONTROL_FULL *CESE_INITIAL_CHEMISTRY

```
$ Setup stochastic particles 
\boldsymbol{\zeta}*STOCHASTIC_SPRAY_PARTICLES 
$ injdist ibrkup icollide ievap ipulse limprt fuelid 
 3 1 0 1 0 100000 1 
$ rhop tip pmass[Kg] prtrte str_inj dur_inj 
 1000.0 300. 0.01 1.0e7 0.0 10.0 
$ the next card is needed for fireball position and max. particle velocity: 
$ XORIG YORIG ZORIG SMR Velinj Drnoz Dthnoz 
 0.005 0.005 1.0e-5 5.0e-6 200.0 9.0e-5 
$ TILTXY TILTXZ CONE DCONE ANOZ AMP0 
 0.0 0.0 15.0 15.0 2.5e-8 0.0 
\ddot{\mathcal{S}}*CHEMISTRY_MODEL 
$ model_id jacsel errlim
```
 10 1 0.0 evap.inp therm.dat tran.dat \ddot{s} *CHEMISTRY_COMPOSITION \$ comp_id model_id $\frac{1}{11}$ 10 \$ molefra Species 1.0 O2 3.76 N2 $\ddot{\mathsf{S}}$ *CHEMISTRY_CONTROL_FULL $$$ $\text{sol}_\text{id}^ \text{errl}\overline{\text{im}}$ 5 \$ \$ \$ Set global initial conditions for fluid $\boldsymbol{\mathsf{S}}$ *CESE_INITIAL_CHEMISTRY \$ sol_id comp_id 5 11 \$INITIAL CONDITIONS \$ uic vic wic ric pic tic hic 0.0 0.0 0.0 1.2 101325. 300.0 0.0

*STOCHASTIC_TBX_PARTICLES

Purpose: Specify particle and other model details for stochastic PDEs that model embedded particles in TBX explosives. Note that the components listed on the corresponding *CHEMISTRY_COMPOSITION card are in terms of molar concentrations of the species (in units of moles/[length]³, where "[length]" is the user's length unit).

For further information on the theory of the TBX model that has been implemented, a document on this topic can be found at this URL:

http://www.lstc.com/applications/cese_cfd/documentation

*STOCHASTIC *STOCHASTIC_TBX_PARTICLES

*STOCHASTIC_TBX_PARTICLES *STOCHASTIC

Remarks:

1. If radiation heat transfer is being modeled, then EMISS and BOLTZ are required.

*LSO

These cards provide a general data output mechanism, causing the creation of a sequence of LSDA files. This facility is intended to allow several different time sequences of data to be output in the same simulation. In addition, any number of domains (and any number of variables on those domains) may be specified within each time sequence. The keyword cards in this section are defined in alphabetical order:

*LSO_DOMAIN

*LSO_ID_SET (not available in the single-precision version of LS-DYNA)

*LSO_POINT_SET

*LSO_TIME_SEQUENCE

*LSO_VARIABLE_GROUP

Note that only the mechanics solver is available in the single-precision version of LS-DYNA, and therefore, only LSO mechanics variables are available for output from single precision LS-DYNA. These mechanics variables are listed by domain type in a separate document. This document (LSO_VARIABLES.TXT) is created by running the command: LS-DYNA print_lso_doc. Contrary to LSO_VARIABLES.TXT, element quantities such as stress are not available for output from the mechanics solver to the "lso" database.

An additional option "**_**TITLE**"** may be appended to all *LSO keywords. If this option is used, then an 80 character string is read as a title from the first card of that keyword's input. At present, LS-DYNA does not make use of the title. Inclusion of titles gives greater clarity to input decks.

*LSO_DOMAIN

Purpose: This command provides a way to specify variables on a subset of the domain for a given solver. This domain can be a subset of the mesh used by that solver, a set of output points created with *LSO_POINT_SET, or a set of objects created with *LSO_**-** ID_SET. The frequency and duration of the output for any given domain is determined by each *LSO_TIME_SEQUENCE card that references this *LSO_DOMAIN card. Note that for the single-precision version of LS-DYNA, the only allowed value of SOLVER_**-** $NAME = MECH.$

Special Domains Card. Card 3 when DOMAIN_TYPE is one of ROGO, CIRCUIT, THIST_POINT or TRACER_POINT.

Miscellaneous Domain Card. Card 3 when DOMAIN_TYPE is one of NODE, PART, SEGMENT, SURFACE_NODE, SURFACE_ELEMENT, VOLUME_ELEMENT, SUR-FACE_PART, VOLUME_PART.

Variable Name Card. Provide as many cards as necessary. This input ends at the next keyword ("*") card

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Remarks:

1. Supported choices for VARIABLE_NAME are listed by DOMAIN_TYPE for each SOLVER_NAME in a separate document. This document (LSO_VARIABLES.TXT) is created by running the command: LS-DYNA print_lso_doc. The following table shows a sample of the point output variables available when DOMAIN_TYPE = THIST_POINT:
*LSO_ID_SET

Purpose: Provides a way to create a set of existing sets (segment sets), or to define a set that is not available with other set-related keyword cards. These are then used in other *LSO cards to specify LSO output. This card is not available in the single precision version of LS-DYNA**.**

Referenced IDs. Provide as many cards as necessary. This input ends at the next keyword ("*") card

VARIABLE DESCRIPTION

SETID Identifier for this ID set.

VARIABLE DESCRIPTION

ID1, … IDs of the TYPE kind.

*LSO_POINT_SET

Purpose: Define a list of points used to sample variables in time. Of the different sampling methods, the most common one is to specify points for time history output.

Point Cards. Provide as many cards as necessary. This input ends at the next keyword $($ "*") card

Remarks:

1. **USE.** For USE = 1, with the ICFD and CESE solvers, the fixed points must remain inside the fluid mesh or a zero result is returned, while for the EM solver, the points can be defined inside the conductors or in the air. In the latter case, the fields will be computed using a Biot-Savart type integration. For USE = 2, a massless tracer particle is tracked for the ICFD and CESE solvers using their local velocity field to integrate the position of each particle in time.

*LSO_TIME_SEQUENCE

Purpose: This command provides users with maximum flexibility in specifying exactly what they want to have appear in the output LSO binary database. Each instance of the ***LSO_TIME_SEQUENCE command creates a new time sequence with an independent output frequency and duration. Furthermore, while the default domain for each output variable will be the entire mesh on which that variable is defined, at all selected snapshot times, the *LSO_DOMAIN keyword commands can be used to specify that output will only occur on a portion of SOLVER_NAME's mesh, and for a limited time interval, or that it will occur at a set of points (see *LSO_POINT_SET), or over a set of object IDs (see *LSO_ID_SET). Note that for the single-precision version of LS-DYNA, the only allowed value of SOLVER_NAME = MECH.

Domain IDs. Provide as many cards as necessary. This input ends at the next keyword ("*") card, or when a global variable name card appears

Global variable names. Provide as many cards as necessary. This input ends at the next keyword ("*") card

Remarks:

1. If LCDT is nonzero, then it is used and DT and NPLTC are ignored. If LCDT is zero and NPLTC is non-zero, then NPLTC determines the snapshot time increment. If LCDT and NPLTC are both zero, then the minimum non-zero time increment specified by DT is used to determine the snapshot times.

*LSO_VARIABLE_GROUP

Purpose: To provide a means of defining a shorthand name for a group of variables. That is, wherever the given group name is used, it is replaced by the list of variables given in this command. Note that for the single-precision version of LS-DYNA, the only allowed value of SOLVER_NAME = MECH.

List Of Variables In Group. Provide as many cards as necessary. This input ends at the next keyword ("*") card

VARIABLE DESCRIPTION

SOLVER_NAME Selects the solver for which data is output in a time sequence.

Remarks:

1. Valid VAR_NAMEs depend both upon the SOLVER_NAME and the DO-MAIN_TYPE. These variables are listed by DOMAIN_TYPE for each SOLV-ER_NAME in a separate document. This document (LSO_VARIABLES.TXT) is created by running the command: LS-DYNA print_lso_doc.